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# Temperature Dependent Characterization and Crystallization Dynamics of Ge<sub>2</sub>Sb<sub>2</sub>Te<sub>5</sub> Thin Films and Nanoscale Structures

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# **Temperature Dependent Characterization and Crystallization Dynamics of $\text{Ge}_2\text{Sb}_2\text{Te}_5$ Thin Films and Nanoscale Structures**

Kadir Cil, Ph.D.

University of Connecticut, 2015

Phase change memory (PCM) is currently seen as the most promising candidate for a future storage-class memory with the potential to be as fast as Dynamic Random-Access Memory but with much longer retention times, and as dense as flash memory but significantly faster due to unique material properties which include strong electrical resistivity contrast, fast crystallization and high crystallization temperature. PCM devices utilize chalcogenide materials (most commonly  $\text{Ge}_2\text{Sb}_2\text{Te}_5$ , or GST) that can be reversibly and rapidly switched between amorphous and crystalline phases (enabling storage of information) with orders of magnitude difference in electrical resistivity. Crystallization dynamics, transition temperatures, and grain size distributions depend on the material composition, interfaces and cell geometry and determine the electrical pulses required for operation, cell performance, power consumption and reliability.

This work focused on temperature dependent characterization of GeSbTe thin films and nanoscale structures with the goal of contributing to a better understanding of phase-change memory materials and devices.

The electrical resistivity of liquid GST ( $\rho_{\text{GST-Lq}}$ ) was extracted from measurements on large number of individual GST nanostructures self-heated to melt by single microsecond voltage pulses, as well as on thin film samples. The crystallization behavior of GST films on silicon nitride and on silicon dioxide through slow resistance

versus temperature measurements was also characterized. Silicon nitride appears to facilitate the fcc-hcp phase-transition of GST and we speculate this may be due to the hexagonal symmetry of silicon nitride. Our results also show the importance of the heating rate in determining phase transition temperatures.

Understanding the crystallization dynamics is critically important for PCM device operation. Above a certain amplitude, a baseline (or offset) voltage after a melting pulse can play an important role in the set operation by leading to retention of a molten filament and growth-from-melt templated from the surrounding crystalline regions. The effect of different baseline voltages on the set dynamics of phase change memory devices was studied by applying melting voltage pulses with varying baseline voltages. Simulations of the effect of different baseline voltages were also performed to compare to and help interpret the experimental results.

Lastly, in-situ X-Ray Diffraction (XRD) measurements up to high temperatures and ex-situ XRD measurements on pre-annealed samples were performed to characterize grain size distributions as a function of anneal temperature. The material crystallizes over time as the chuck temperature is increased and the crystallization process is monitored by the evolution of different peaks in the XRD measurement which are related to the grain sizes. These results will be used to improve and calibrate our electrothermal and crystallization models for PCM materials and devices.

**Temperature Dependent Characterization and Crystallization  
Dynamics of Ge<sub>2</sub>Sb<sub>2</sub>Te<sub>5</sub> Thin Films and Nanoscale Structures**

Kadir Cil

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A Dissertation  
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at the  
University of Connecticut  
2015

# APPROVAL PAGE


Doctor of Philosophy Dissertation

## **Temperature Dependent Characterization and Crystallization Dynamics of Ge<sub>2</sub>Sb<sub>2</sub>Te<sub>5</sub> Thin Films and Nanoscale Structures**

Presented by

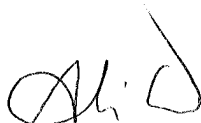
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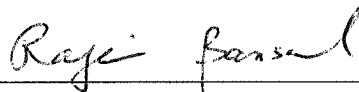
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## 1. Introduction

Demand for high-speed, high-density and low-power computation, and expected limitations in scaling of silicon based memory technologies have given rise to investigation of alternative complementary memory technologies such as phase change memory (PCM). PCM is currently seen as one of the most promising candidates for a future storage-class memory [1] with the potential to be almost as fast as Dynamic Random-Access Memory but with much longer retention times (non-volatile), and as dense as flash memory but significantly faster. A possible non-volatile DRAM replacement (no need for refresh and data stored without power supplied) is especially interesting and it could lead to completely new computer architectures. Meanwhile, NAND flash has successfully continued scaling to  $< 20$  nm gate length and 3D V-NAND (with vertical integration of 32 layers of planar NAND) is now being produced by Samsung [2]. PCM has recently entered the market as a lower-density but significantly higher-speed non-volatile memory for mobile applications [3, 4]. PCM's advantage of single bit alterability over flash memory (which requires block-erase to rewrite) makes it a lower-power alternative for certain applications such as code execution [5]. Storage class memory applications such as server and hard drive replacement, require high endurance (number of cycles) while maintaining the fast switching [6]. PCM has much lower latency and higher endurance than NAND flash ( $10^6$  for PCM and  $\sim 3 \times 10^4$  NAND flash) which makes it a well-positioned candidate for server and storage systems where a small amount of PCM can be integrated (hybrid structure) to the speed of the system [7].

Current pulses for the set and reset operations are provided through access device (transistors, diodes) which typically need to be larger than the PCM element itself to provide sufficient current and thus limit the memory packing density. One of the goals to optimize cell design is to reduce the reset current which leads to reduced size of access device, larger storage density and also higher cycling (reduced material damage from lower currents). PCM devices are expected to scale below 10 nm element size with potential for multi-bit/cell storage [8, 9] making PCM promising for non-volatile random access memory implementations if the cells can be operated reliably for very large number of cycles [10].

PCM devices utilize chalcogenide materials (most commonly GeSbTe, or GST [11]) that can be reversibly and rapidly switched between amorphous and crystalline phases with orders of magnitude difference in electrical resistivity. A typical PCM device (mushroom cell) consists of a thin layer of a phase-change material sandwiched between a narrow bottom contact (usually referred to as the heater) and a planar top contact. The active region is a GST semi-sphere above the heater that is switched between the amorphous and crystalline states by a suitable electrical pulse.

Amorphization is obtained by a large amplitude and short electrical pulse that heats the active region above its melting temperature and allows it to cool faster than the crystallization time to re-solidify as amorphous. Crystallization can be obtained by a smaller amplitude and longer duration pulse that heats the active region above its crystallization temperature ( $T_{\text{cryst}}$ ) for a sufficiently long period. Fast crystallization can also be obtained at high temperatures, close to melting, or upon slower cooling from melting. Since the resistivity of the amorphous region is very large, sufficient current

flow for Joule heating and crystallization is obtained with voltage pulses that are high enough to initiate electrical breakdown (threshold switching). In GST films, the room-temperature electrical resistivity changes by a factor of  $\sim 10^5$ - $10^6$  between the amorphous and crystalline phases. Viable PCM operation and scaling require melting of a very small volume of phase-change material in a very short time period with minimum possible energy, while ensuring reliability over the lifetime of the device and a large number of melting and solidification cycles ( $\sim 10^9$ ) [7]. Operation of the PCM cell also depends on the choices of the substrate and thickness of the phase change material. We have compared the crystallization behavior of GST films on different substrates with varying GST film thickness under different heating rates. The measurements demonstrate that crystallization temperature can increase or decrease depending on substrate material and film thickness and the difference can be as large as 80 K for second transition temperature (from *fcc* to *hcp*).  $\text{Ge}_2\text{Sb}_2\text{Te}_5$  (GST) is the most common phase change material due to its crystallization times, stability of amorphous phase and large resistivity contrast between the amorphous and crystalline phases [12]. In small-scale PCM devices, in which the active region is repeatedly switched between amorphous and face-centered cubic (*fcc*) phases, an overall resistance ratio of  $\sim 100$ -1,000 is typically obtained with switching times  $\sim 50$ -100 ns [11].

### **1.1 Material parameters for phase change memory device modeling**

PCM elements experience large range of operation temperatures and thermal gradients ( $\sim 10$ -100 K/nm) while switching between crystalline, liquid and amorphous phases. Crystallization is materialized by reorganization of atoms and bonding mechanisms at the molecular level. Crystallization dynamics and transition

temperatures depend on the composition, interfaces and cell geometry and determine the required electrical pulses used for operation, which in turn impact cell performance, power consumption and reliability [13]. Rigorous device modeling that can enable further scaling and evaluation of device failure mechanisms, requires well-determined materials parameters in the whole operation range including the liquid state. The temperature dependent material parameters used in the modeling studies shown in this thesis are shown in Figure 1.1 [14-16].

Electrical resistivity ( $\rho$ ) and thermal conductivity ( $\kappa$ ) as a function of temperature of TiN are obtained from Gottlieb et al. [17] and Shackelford et al. [18] respectively (Figure 1.1a). Heat capacity and Seebeck coefficient of TiN are assumed to have constant values of 784 J/kg.K and 1  $\mu$ V/K. [19, 20].

Thermal boundary resistances (TBR) at the GST-TiN, GST-SiO<sub>2</sub>, and TiN-SiO<sub>2</sub> interfaces are obtained by adding 1 nm thick virtual layer at each boundaries with a temperature dependent thermal boundary conductivity (TBC). TBR at GST-TiN interface is ~20 m<sup>2</sup>K/GW between 300 K and 600 K and it decreases significantly due to increased electronic contribution of thermal conductivity when the phase change material approaches melting temperature. TBR at GST- SiO<sub>2</sub> interface is negligible up to melting temperature of GST. When the GST melts and becomes highly conductive TBR increases to ~20 m<sup>2</sup>K/GW, typical value for metal-insulator interface. TBC between TiN and SiO<sub>2</sub> is assumed to be constant: 0.05 W/(m.K) as these materials do not change phase in that temperature range (Figure 1.1b) [21, 22].

Temperature dependent electrical resistance of amorphized and *fcc* GST wires are measured from 300 K up to 675 K with 1K/min heating rate. The resistivity values are



calculated by using actual device dimensions. Up to first crystallization temperature ( $\sim 420$  K) crystallization time scale is comparable for slow measurements. At elevated temperatures crystallization is faster and resistivity of the material becomes a function of temperature and heating rate. Therefore, GST retains a metastable crystalline state during reset operation because the heating rate is faster than crystallization time. The calculated exponential decay of resistivity values for amorphous and *fcc* GST are extrapolated up to melting temperature to model the metastable resistivity functions [15, 16, 23-26]. Liquid-GST resistivity values used in the simulations are from the experimental results obtained by Cil et al. [14] (Figure 1.1c).

Room-temperature values of the thermal conductivity ( $\kappa$ ) of GST as obtained from the literature are considered to be purely due to phonon conduction [22, 27-29]. This term is assumed to be decreasing linearly with GST resistivity, whereas the electronic contribution is calculated to be increasing with temperature following the Wiedemann-Franz law which relates the thermal conductivity and the electrical conductivity of a metal. Total thermal conductivity is calculated as sum of the phonon and electronic components. Thermal conductivity of liquid GST is assumed to be dominated by the electronic conduction due to the large electrical conductivity (Figure 1.1d); contributions from convection in liquid phase are not accounted for [23].

The heat capacity ( $C_p$ ) of GST is obtained from both Yin et al. [19] and Liu et al. [20] as a constant value of 202 J/(kg.K). Latent heat of fusion of GST is accounted for by a 10 K spike in the heat capacity function for the heat required for solid to liquid phase-change. A 10 K phase-change range is preferred for ease of simulations, instead of a more sudden transition (Figure 1.1e).

Seebeck coefficient ( $S$ ) of amorphous and  $fcc$  phases GST were measured by Adnane et al. [30] from room temperature up to 740 K in our laboratory.  $S(T)$  is extrapolated to be constant between 740 K and melting temperature (873 K) and assumed to have a small constant value of 1  $\mu\text{V/K}$  in the liquid phase (Figure 1.1f) [31].

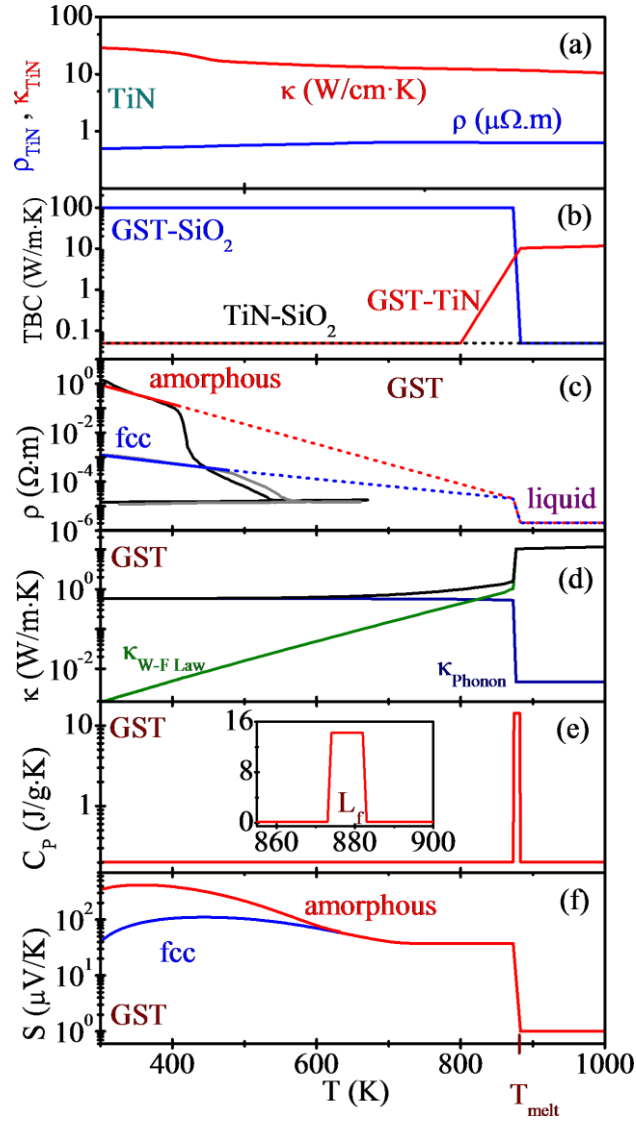


Figure 1.1. Temperature dependent electrical and thermal conductivities of TiN (a), thermal boundary conductivities between GST-SiO<sub>2</sub>, GST-TiN and TiN-SiO<sub>2</sub> (b), electrical resistivities of amorphous and  $fcc$  GST (c), thermal conductivity of GST (calculated electronic and estimated phonon contributions) (d), Heat capacity of GST

around the melting temperature (e), inset showing the peak to incorporate the latent heat of fusion, and Seebeck coefficient of amorphous and fcc GST (f)[15, 16, 23, 24, 30, 32]

## 2. Electrical Resistivity of Liquid GST

Electrical resistivity of liquid  $\text{Ge}_2\text{Sb}_2\text{Te}_5$  is obtained from DC current-voltage measurements performed on thin  $\text{Ge}_2\text{Sb}_2\text{Te}_5$  films as well as from device level micro-second pulse voltage and current measurements performed on two arrays (thickness:  $20 \pm 2$  nm,  $50 \pm 5$  nm) of lithographically defined encapsulated  $\text{Ge}_2\text{Sb}_2\text{Te}_5$  nano/micro-wires (length: 315 nm to 675 nm, width: 60 nm to 420 nm) with metal contacts. Thin film measurements yield  $1.26 \pm 0.15$  m $\Omega$ .cm (thickness: 50, 100 and 200 nm), however, there is significant uncertainty regarding the integrity of the film in liquid state. The device level measurements utilize melting of the encapsulated structures by a single voltage pulse while monitoring the current through the wire. Melting is verified by stabilization of current during the pulse. The resistivity of liquid  $\text{Ge}_2\text{Sb}_2\text{Te}_5$  is extracted as  $0.31 \pm 0.04$  m $\Omega$ .cm and  $0.21 \pm 0.03$  m $\Omega$ .cm from 20 nm and 50 nm thick wires arrays.

PCM utilizes the large electrical resistivity contrast between the amorphous and the crystalline phases of phase change materials (typically chalcogenides [11]), which can be reversibly and rapidly switched between the two phases by self-heating via electric pulses. A typical PCM device (mushroom cell) consists of a thin layer of a phase-change material sandwiched between a narrow bottom contact and a planar top contact (Figure 2.1). Amorphization is obtained by a large amplitude and short pulse which melts a small semi-spherical volume of material covering the contact area and allows it to freeze quickly. Crystallization is achieved by either using a smaller amplitude and longer duration pulse which heats the amorphized region above the crystallization temperature ( $T_{\text{cryst}}$ ) for a sufficiently long period or melting followed by slower cooling. Since the resistivity of the amorphous region is very large, sufficiently large voltage pulses are

needed to initiate electrical breakdown (threshold switching) for crystallization.

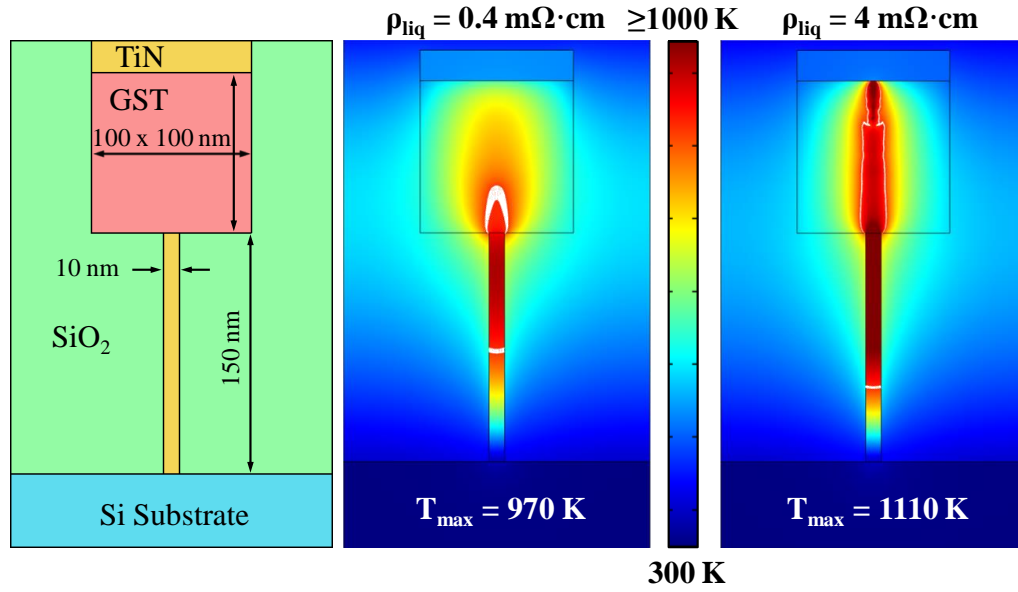


Figure 2.1. Simulated mushroom phase-change memory device and the two distinctly different simulated temperature profiles, using the two previously reported values for electrical resistivity of liquid GST ( $\rho_{\text{GST-Lq}} \sim 0.4 \text{ m}\Omega\cdot\text{cm}$  [33] and  $\sim 4 \text{ m}\Omega\cdot\text{cm}$  [34]). Temperature-dependent materials parameters, latent heat of fusion upon melting, thermoelectric contributions and thermal boundary resistances are included in this model [15, 23]. The lowest temperature is 300 K. The white contour lines indicate the solid-liquid transition temperature range (assumed as 873-883 K), within which GST is in the liquid state.

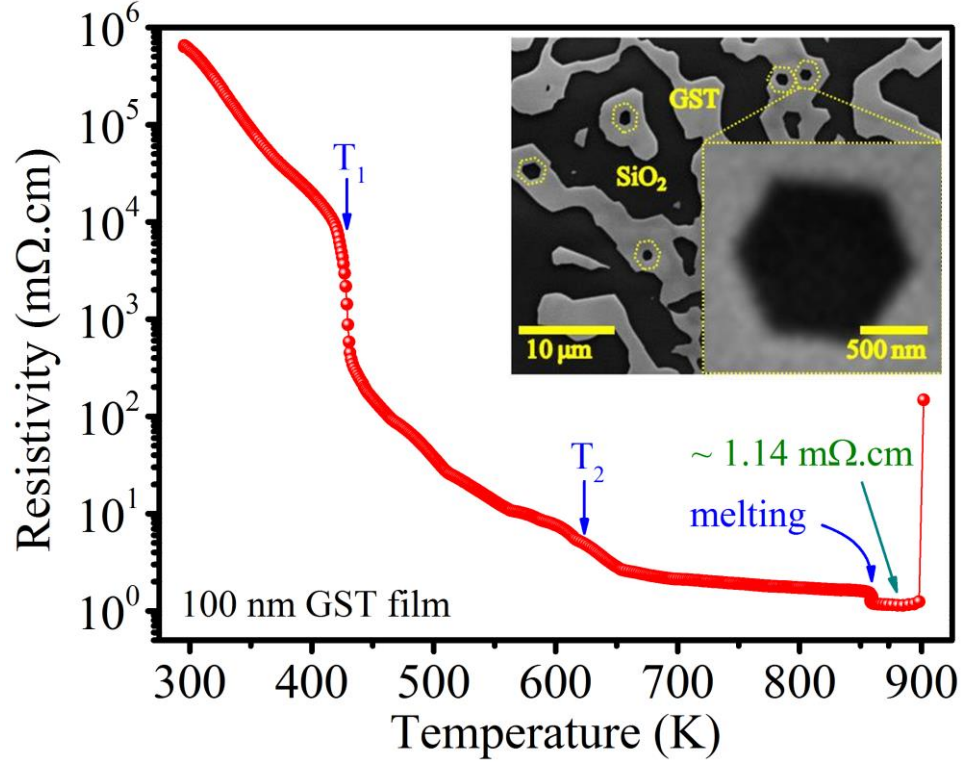


Figure 2.2. Resistivity of a 100 nm thick amorphous GST film, measured up to 900 K. The sudden increase at 900 K indicates losing contact with the film. The arrows indicate transitions from amorphous to *fcc* ( $T_1 \sim 428$  K), from *fcc* to *hcp* ( $T_2 \sim 637$  K) and from *hcp* to liquid (melting  $\sim 858$  K). Inset SEM image shows a segment of a 100 nm thick GST film which has been heated up to 875 K. The GST film breaks apart in liquid phase, possibly due to surface tension and form hexagonal boundaries upon resolidification.

Even though GST is the most studied phase change material, at the time of this publication there were only two reports on the electrical resistivity of liquid GST ( $\rho_{\text{GST-Lq}}$ ) in the literature (with significant disparity):  $\rho_{\text{GST-Lq}} \sim 4$  mΩ.cm based on measurements on a 110 nm thick GST film [34];  $\rho_{\text{GST-Lq}}$  varying from  $\sim 0.41$  mΩ.cm at 930 K to  $\sim 0.36$  mΩ.cm at 990 K based on temperature dependent measurements on molten GST ( $T_{\text{melt}} = 873$  K) in a macroscopic setup [33]. Thermal conductivity of liquid

GST ( $k_{GST-Lq}$ ) is expected to be dominated by its electronic component (metallic behavior) and can be estimated using the  $\rho_{GST-Lq}$  value and Wiedemann-Franz (W-F) Law ( $k_{GST-Lq} = LT/\rho_{GST-Lq}$ ,  $L$  = Lorenz Number). Similarly thermal boundary resistances (TBR) at liquid GST interfaces with other materials are also estimated based on W-F Law and the  $\rho_{GST-Lq}$  value [15]. Hence, the  $\sim 10x$  disparity in the reported values, which may be caused by measurement errors, compositional differences, or thickness dependence, has a significant impact on predicted device operation dynamics (Figure 2.1).

## 2.1 Thin Film Measurements

We have performed room temperature resistivity measurements using the Van der Pauw method and four-point resistance versus temperature measurements on thin GST films with patterned metal contacts (going above  $T_{melt}$ ) and obtained  $\rho_{GST-Lq}$  as 1.43 m $\Omega$ .cm for 50 nm, 1.14 m $\Omega$ .cm for 100 nm, 1.22 m $\Omega$ .cm for 200 nm thick films, averaging  $1.26 \pm 0.15$  m $\Omega$ .cm (Figure 2.2). We have observed that the films typically do not maintain their integrity during the measurement, possibly due to surface tension, and form hexagonal micro-structures upon resolidification, suggesting crystallization in hexagonal close pack (*hcp*) phase (Figure 2.2 inset). Hence, thin film measurements are not reliable enough to extract  $\rho_{GST-Lq}$  for rigorous device modeling and device level  $\rho_{GST-Lq}$  measurements, in which the liquid can be contained, are necessary to verify the reported values and determine if there are any size effects.

## 2.2 Device Level Measurements

The electrical measurements were performed in a Janis vacuum probe station [35] with temperature control (up to 680 K), under high vacuum ( $10^{-5}$  torr) that minimizes

oxidation of the structures. The samples were clamped to the chuck for good thermal contact and temperature was measured using an E-type thermocouple clamped to the chuck. The slow (1 K/min ramp rate) R-T characteristics (300 K to 680 K) of an as-fabricated wire (*fcc*) and a pulse-amorphized wire (at room temperature, using 500 ns, 2.2 V pulse) were simultaneously measured by continuously sweeping the applied voltages in  $\pm 100$  mV range using an Agilent 4156C semiconductor parameter analyzer (Figure 2.3). The amorphous wire transitions to *fcc phase* at  $\sim 420$  K ( $T_{fcc}$ ) and both wires transition from *fcc* to hexagonal-close-packed (*hcp*) phase at  $\sim 640$  K ( $T_{hcp}$ ).

We have extracted  $\rho_{GST-Lq}$  from electrical pulse measurements [36] on a large number of GST nano/micro-wires with bottom metal contacts fabricated using conventional photolithography and semiconductor processing techniques on bulk Si wafers with  $\sim 700$  nm thermally grown  $SiO_2$  (Figure 2.4 a). 250 nm deep trenches were etched into the  $SiO_2$  layer using reactive ion etching (RIE), which were filled with a 300 nm layer of titanium nitride (TiN) using chemical vapor deposition (CVD) and physical vapor deposition (PVD) systems (Figure 2.4 b, c). The wafers were then polished using chemical and mechanical polishing (CMP) to achieve planar bottom contacts (Figure 2.4 d). Undoped, stoichiometric  $Ge_2Sb_2Te_5$  films ( $20 \pm 2$  nm and  $50 \pm 5$  nm) were deposited by co-sputtering from elemental targets at low temperature (amorphous phase) (Figure 2.4 e), followed by sputter deposition of a 10 nm silicon dioxide ( $SiO_2$ ) cap layer. The GST wire structures were then patterned using optical lithography and RIE (Figure 2.4 f) with lengths (L) varying from 315 to 675 nm and widths (W) varying from 60 to 420 nm, in 20 nm increments. A 15 nm silicon nitride ( $Si_3N_4$ ) blanket layer is then deposited by plasma-enhanced chemical vapor deposition (PECVD) at 200 °C to encapsulate the



structures (Figure 2.4 g, h). Since the crystallization temperature of GST is  $\sim 150^\circ\text{C}$ , the structures are expected to transition from amorphous to fcc phase during this final PECVD deposition step. The resulting device dimensions were measured by SEM.

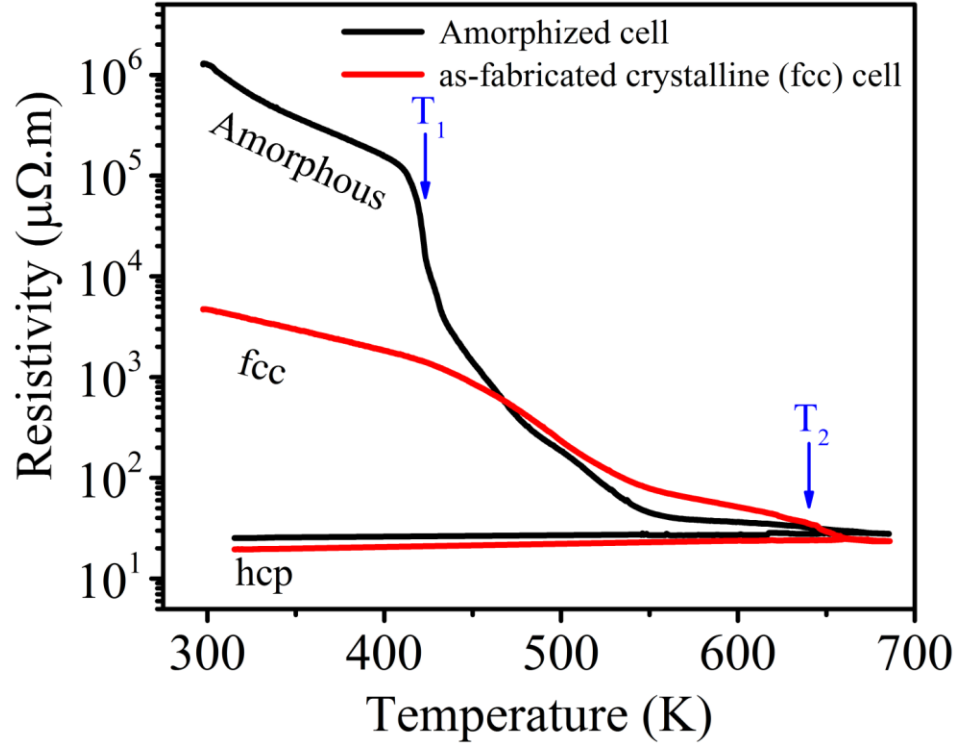


Figure 2.3. Resistivity as a function of temperature for an  $L \times W \times t = 460 \text{ nm} \times 160 \text{ nm} \times 50 \text{ nm}$  pulse-amorphized GST line-cell (using 500 ns, 2.2 V, at room temperature) and an as-fabricated *fcc* GST line-cell  $L \times W \times t = 460 \text{ nm} \times 255 \text{ nm} \times 50 \text{ nm}$ . The arrows indicate transition temperatures from amorphous to *fcc* ( $T_1 \sim 420 \text{ K}$ ) and from *fcc* to *hcp* ( $T_2 \sim 640 \text{ K}$ ).

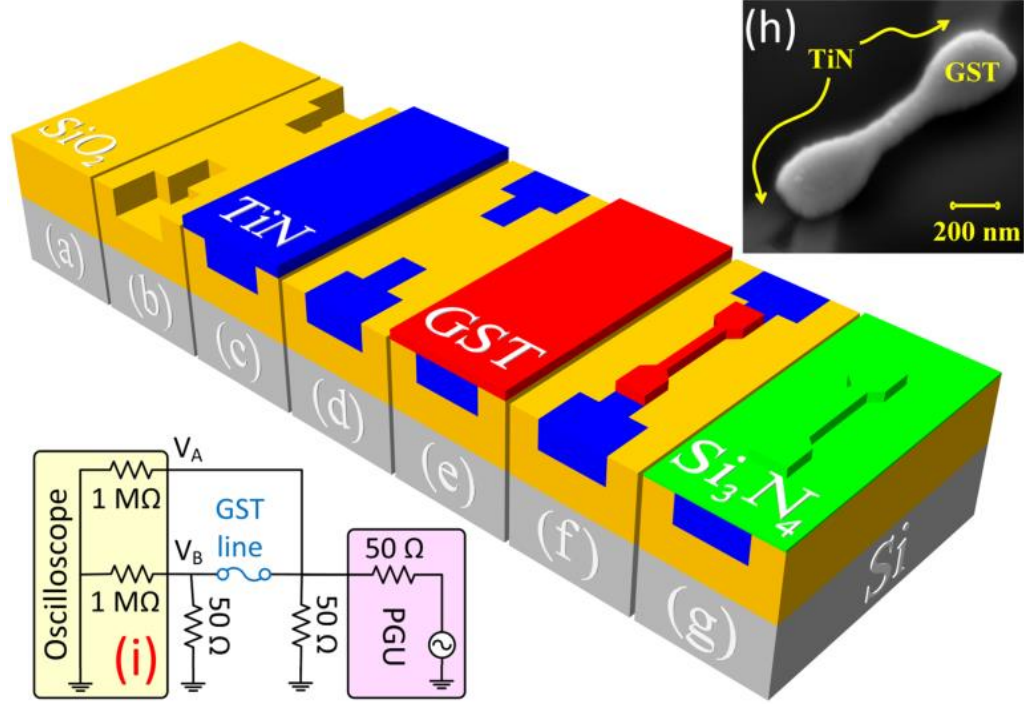


Figure 2.4. Schematics of the fabrication processes of the GST line structures on 700 nm SiO<sub>2</sub> grown on Si (a), after 250 nm deep trench formation (b), 300 nm TiN fill (c), CMP (d), GST film deposition (e), patterning of GST film (f), and Si<sub>3</sub>N<sub>4</sub> cap layer deposition (g). SEM image of a fabricated line structure (h) and the schematic of the experimental setup (i).

Liquid state measurements ( $\rho_{\text{GST-Lq}}$ ) were performed by melting the wires via self-heating with short voltage pulses (Figure 2.5) since the chuck can only be heated to  $\sim 680$  K  $< T_{\text{melt}} = 873$  K. An Agilent 8114A pulse generator (PGU) and a Tektronix DPO4104 oscilloscope are configured as in Figure 2.4 (i) for the pulse measurements, using short coaxial cables for connections. 1 to 1.9 V pulses with 1  $\mu$ s duration and 0.2 V baseline offset are applied to fully melt GST wires of varying sizes. Complete melting of the structures is observed as a plateau in the current during the pulse (Figure 2.5)[36]. The structures used in these measurements are narrow ( $\sim 60$ -600 nm) and  $\sim 60\%$  of the wires are completely broken by the pulse after melting. The current levels are stable in the

liquid state prior to sudden breaking of the wires, which indicates that the wires are completely molten and there is no molten filament that is widening or narrowing over time. The baseline voltage is used to measure the wire resistance before and after the pulse without significant self-heating. The sample temperature was kept at 500 K ( $> T_{fcc}$ ) to observe crystallization of the amorphized wires (after amorphization pulses) and verify integrity of the structures.

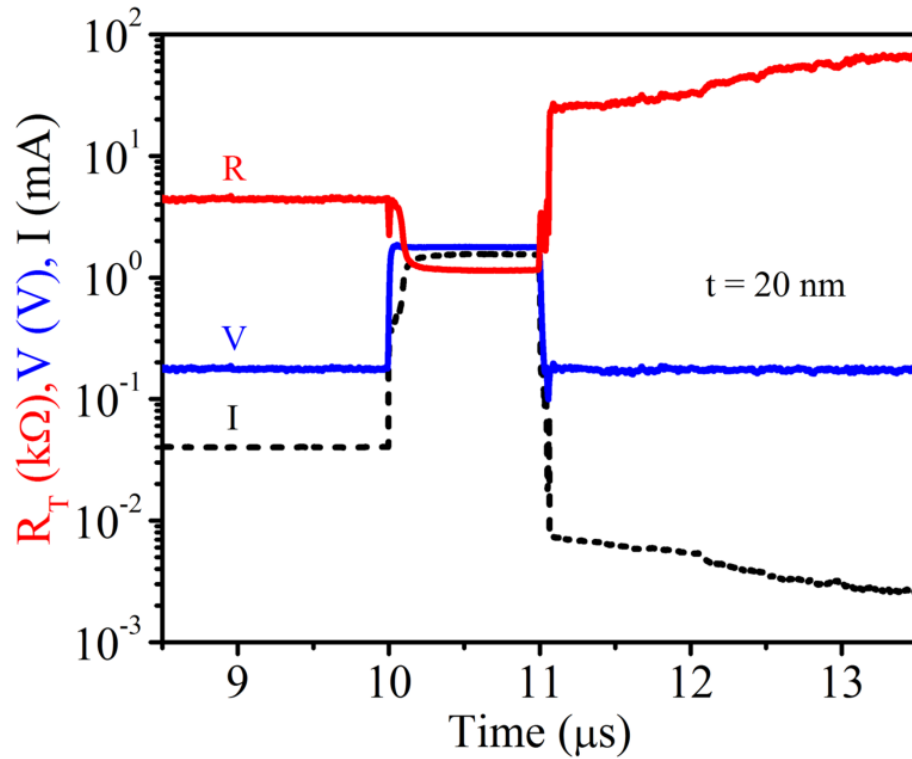


Figure 2.5. Measured voltage ( $V_A$ ), current ( $V_B/50 \Omega$ ) and total resistance ( $R_T$ ) as a function of time for an  $L \times W \times t = 615 \text{ nm} \times 180 \text{ nm} \times 20 \text{ nm}$  GST line.  $T=500 \text{ K}$ .  $I(t)$  and  $V(t)$  data are smoothed using a 1,000 point adjacent averaging. After the pulse the line is amorphized and the current levels are too low to be accurately measured by the oscilloscope due to significant voltage offsets [37]. The actual resistance is expected to be 10x higher than what could be measured. The baseline voltage used to measure resistance leads to sufficient current flow and self-heating to keep the wire above ambient

temperature, hence resistance in amorphous state is observed to be increasing gradually after the melting pulse. The metastable amorphous state is significantly more conductive at elevated temperatures. Crystallization time at 500 K is  $\sim 1000$  s [38] and recrystallization of the wire is not captured in the 20 microsecond duration of this measurement.

Self-heating in the melted region is limited due to reduced resistivity upon melting and temperature stabilization at the liquid-solid interfaces at  $T_{\text{melt}}$  due to absorption of latent heat of fusion. The temperature variation within the melt is expected to be small due to large electronic thermal conductivity in metallic liquid phase enhanced by convection in liquid state [39]. Hence, the temperature of the melt is expected to remain relatively close to  $T_{\text{melt}}$  in these experiments. In addition, the reported temperature coefficient of resistivity (TCR) of liquid GST from bulk measurements is small,  $\sim -0.8$   $\mu\Omega\cdot\text{cm}/\text{K}$  at 990 K [33], hence the variations in liquid state resistivity obtained by this method due to the temperature rise within the molten volume are expected to be relatively small.

### 2.3 Results and discussion

Figure 2.5 shows an example of the measured voltage ( $V_A$ ), output current ( $I = V_B / 50\Omega$ ) and corresponding total resistance of a line cell ( $R_T = (V_A - V_B) / I$ ) during a 1  $\mu\text{s}$ , 1.6 V pulse ( $L \times W \times t = 615 \text{ nm} \times 180 \text{ nm} \times 20 \text{ nm}$ ). The pulse voltage is constant after a short transient period while the measured current has a characteristic non-linear response until it reaches the maximum value (Figure 2.5). This non-linear behavior is expected to be a combined effect of the negative temperature coefficient of resistance of GST and dynamically changing power transfer conditions [40] as the structure starts melting. Once

a contact-to-contact liquid GST path forms, the resistance reaches a steady state (plateau) and all reactive current contributions are eliminated. The measured total resistance ( $R_T$ ) at the plateau includes the  $50\ \Omega$  terminator, the TiN metal extension resistances ( $R_M \approx 200\ \Omega$ ) and the GST wire resistance ( $R_{GST}$ ) (2.2).  $R_{GST}$  includes  $R_x$ , the common contributions arising from contact pads and TiN/GST interface contact resistance (2.2).

$$R_T = R_{GST} + R_M + 50\Omega \quad (2.1)$$

$$R_{GST} = \rho \frac{L}{Wt} + R_x \quad (2.2)$$

$R_T$  at the plateau is plotted as a function of  $1/W$  for devices with different  $L$  (Figure 2.6). The y-intercept of the linear fits made for each  $L$  indicate contact resistance values common to all wires ( $R_x = 114 \pm 32\ \Omega$  for  $t = 20\ \text{nm}$  and  $98 \pm 27\ \Omega$  for  $t = 50\ \text{nm}$ ). The slopes of these fits ( $\alpha = \rho.L/t$ ) are then plotted as a function of  $L$  for both thicknesses (Figure 2.7). The slopes of these second fits ( $\beta = \rho/t$ ) are used to extract the liquid state resistivity,  $\rho_{GST-Lq}$ , as  $0.31 \pm 0.04\ \text{m}\Omega.\text{cm}$  for  $t = 20\ \text{nm}$  and  $0.21 \pm 0.03\ \text{m}\Omega.\text{cm}$  for  $t = 50\ \text{nm}$ . The calculated errors have contributions from the error in regression for  $\beta$ , which accounts for the error in regression for  $\alpha$  values (shown as error bars in Figure 2.7) and the error in thickness (estimated as  $\sim 10\%$  based on SEM imaging). The difference between the results obtained from 20 nm and 50 nm thick structures may be due to variations in the melting of the wider pad region, impact of pressure or surface cooling effects for the two thicknesses.

The extracted values of  $0.31 \pm 0.04\ \text{m}\Omega.\text{cm}$  and  $0.21 \pm 0.03\ \text{m}\Omega.\text{cm}$  from 20 nm and 50 nm thick structures using this device level approach are close to those reported by

Endo et al. from large-scale measurements of liquid GST ( $\sim 0.36 \text{ m}\Omega\cdot\text{cm}$  at  $\sim 990 \text{ K}$  with a TCR of  $-0.8 \text{ }\mu\Omega\cdot\text{cm/K}$  [33]). This extracted liquid resistivity value is also comparable to resistivity of the *hcp* phase at melting temperature (Figure 2.2).

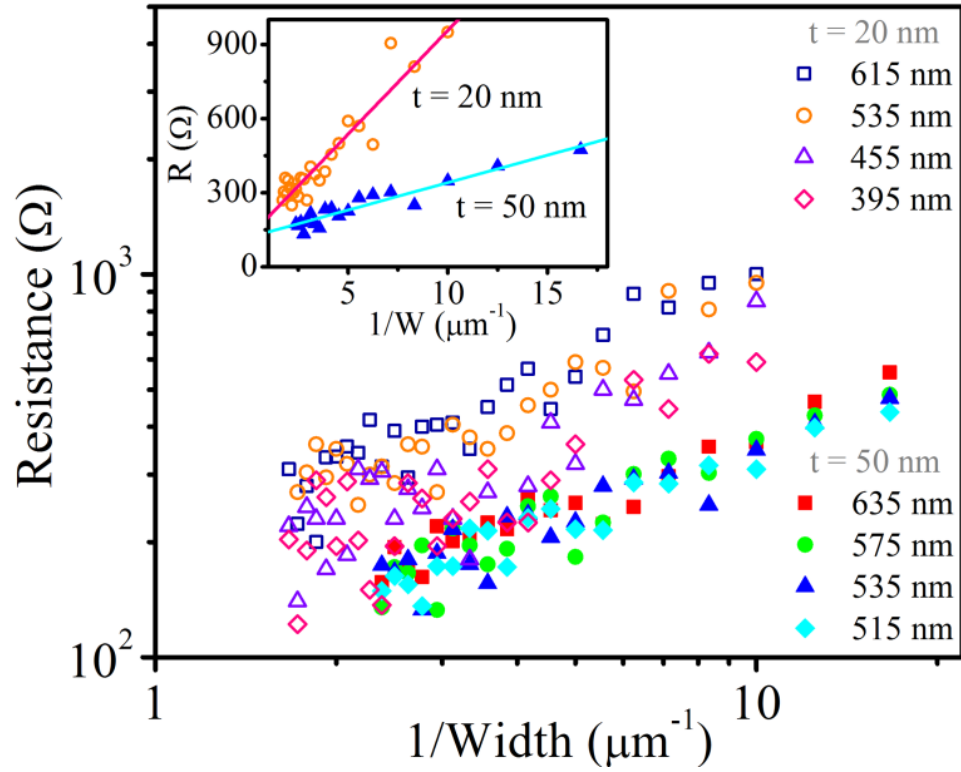


Figure 2.6. GST resistance ( $R_{\text{GST}}$ ) during pulse versus reciprocal of line width in logarithmic scales for 4 different  $L$ , for  $t = 20 \text{ nm}$  ( $W = 60$  to  $420 \text{ nm}$  in  $20 \text{ nm}$  increments),  $t = 50 \text{ nm}$  ( $W = 100$  to  $600 \text{ nm}$  in  $20 \text{ nm}$  increments). Inset shows the  $L = 535 \text{ nm}$  and linear fits for both thicknesses.

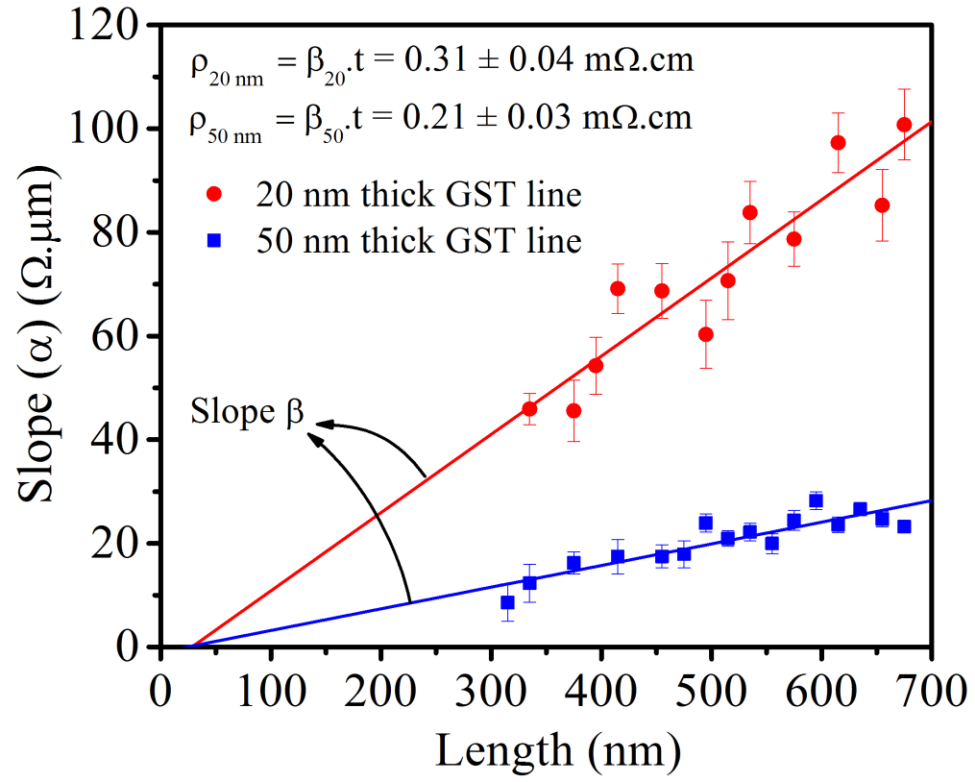


Figure 2.7. Slopes ( $\alpha$ ) obtained from the fits in Fig. 6 versus  $L$  and linear fits for two different thicknesses (20 and 50 nm) of GST lines.

### **3. Assisted cubic to hexagonal phase transition in GeSbTe thin films on silicon nitride**

The amorphous to face-centered cubic (fcc) and fcc to hexagonal close-packed (hcp) crystallization temperatures of GeSbTe thin films on underlying silicon nitride and silicon dioxide films were studied through slow (1 K/min) resistance versus temperature measurements. The amorphous to fcc phase transition is observed at ~ 170 °C for both cases but the fcc to hcp phase transition temperature for GeSbTe films on silicon nitride is observed ~ 80 °C lower than for GeSbTe films on silicon dioxide, possibly due to the hexagonal symmetry of silicon nitride.

#### **3.1 Introduction**

The crystallization behavior of the phase change material determines the power required for switching, programming speed, retention time and also affects other important device properties such as reliability and device-to-device variability. It has been observed that the crystallization behavior of phase change materials depends strongly on chemical composition [41], structure, heating rate [42], cladding materials [43], doping, and even thickness or device size [12]. GST undergoes a first phase transition from amorphous to fcc and a second phase transition from fcc to hexagonal close-packed (hcp) [44]. Most research to date has focused on the amorphous-cubic phase transition [12, 45, 46]. Since in PCM devices the active region traverses the whole temperature range from room temperature to melting temperature (~ 600 °C for GST), detailed knowledge of the second transition (fcc to hcp) and the solid to liquid transition is also crucial.



It has been reported that for GST films sandwiched between silicon dioxide layers the amorphous-fcc transition temperature increases with decreasing thickness from  $\sim 150$  °C for 50 nm thick films to  $\sim 250$  °C for thinner films (thinnest  $\sim 2.5$  nm) but the fcc-hcp transition temperature increases slightly with increasing thickness, from 320 °C for the thinner films to 340 °C for the thicker films [12]. We have also recently shown that, for GST films thicker than 10 nm on silicon nitride, the amorphous-fcc phase transition is observed at approximately the same temperature for all film thicknesses but the fcc-hcp transition is observed at higher temperatures for thicker films [47]. These results suggest the GST-silicon nitride interface plays a role in promoting the fcc-hcp transition.

In this work we test this hypothesis by comparing the amorphous-fcc and fcc-hcp crystallization temperatures of GST thin films on silicon nitride (GST/nitride) and on silicon dioxide (GST/oxide) through electrical resistance versus temperature (R-T) measurements. Auger Electron Spectroscopy (AES) was also used to compare any compositional differences between the GST films on oxide and nitride.

### **3.2 Experimental details**

Stoichiometric GST ( $\text{Ge}_2\text{Sb}_2\text{Te}_5$ ) thin films with target thicknesses of 10, 20, 50 and 100 nm were deposited by co-sputtering from elemental Ge, Sb and Te targets over silicon nitride ( $\sim 50$  nm) on oxidized ( $\sim 300$  nm silicon dioxide) single-crystal silicon substrates, or directly over oxidized silicon substrates ( $\sim 300$  nm silicon dioxide). The GST film deposition condition was developed and calibrated using Rutherford Backscattering spectrometry as described in Ref.[45]. GST films thicknesses were measured by Transmission Electron Microscopy (TEM) cross-

sectional analysis as 11 nm for the thinnest film of GST (GST/nitride, target of 10 nm GST) and 87 nm for the thickest film of GST (GST/nitride, target of 100 nm GST). For all other samples, a similar percent deviation from target thickness is expected. The GST/oxide samples are capped by a 10 nm layer of silicon dioxide to prevent oxidation and evaporation of GST at high temperatures. The measured films stacks, from surface to substrate are then GST/SiN/SiO<sub>2</sub>/Si for the GST/nitride samples (Figure 3.1 a) and SiO<sub>2</sub>/GST/SiO<sub>2</sub>/Si for the GST/oxide samples (Figure 3.1 b).

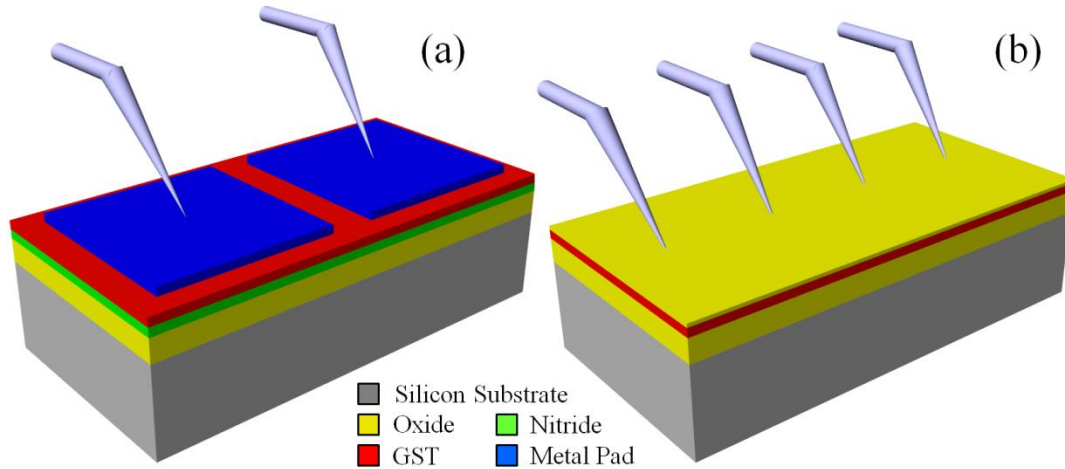


Figure 3.1. Schematics of a GST/nitride sample with contact pads used for two-point R-T measurements (a) and a GST/oxide sample directly probed for four-point R-T measurements (the probes can easily scratch the 10 nm capping silicon dioxide) (b). Films, contact pads and probes are not drawn to scale for visibility. The GST films are 10, 20, 50 or 100 nm and the underlying silicon dioxide and silicon nitride are 300 nm and 50 nm respectively.

The GST/nitride samples have large area contact pads (~ 50 nm thick), formed by platinum deposition on the capped GST films through a metal shadow mask or in some cases, by manual definition of similar sized contacts using graphite paste. For these samples, the electrical resistance was measured between two contacts.

The GST/oxide samples do not have contacts and the electrical resistance was measured using four-point configuration by directly probing the blanket films with tungsten micro-positioned tips approximately linearly and equally spaced. In all 50 nm GST/oxide samples the GST film was patterned by deposition through a contact mask; the resistance was also measured using four probe configuration for these samples.

To eliminate the possible effect of different contacts used for the GST/nitride and GST/oxide samples, one GST/nitride sample (50 nm) was also measured using four-point probe configuration with the probes applied directly to the film. The different contact types and measurements are indicated in the figures.

The measurements were performed in a cryogenic micro-manipulated probe station chamber (~ 20" internal diameter) under high vacuum ( $10^{-3}$  -  $10^{-4}$  Pa) to prevent oxidation of the films. The probe station allows temperature control up to ~ 680 K. The contact pads (or sample surface in the four-point measurement cases) were probed using tri-axial probe arms with tungsten needles and the current and voltage were measured using an Agilent 4156C Parameter Analyzer. The glass window of the chamber lid is covered to minimize the contribution of photoconductivity, especially in the amorphous phase where it is more significant. Current-voltage (I-V) characteristics show linear behavior, indicating ohmic contact between the probes and the contact pads or the GST films.

The resistance is obtained from I-V data measured using the parameter analyzer. Approximate resistivity values are obtained from the measured resistance for each sample, for comparison of samples with different thickness or contacts separation. For the two-point measurements, the resistivity was calculated as  $\rho = R.A/l$

(assuming negligible fringe fields), where  $R$  is the measured resistance,  $A$  is the cross-section area (contact width (0.8mm) x film thickness) and  $l$  is the contact pads separation (0.25 mm). For the four-point measurements, the resistivity was extracted using  $\rho = \pi.t/\ln(2).(V/I)$  where  $t$  is the film thickness,  $V$  is the voltage between the two inner probes and  $I$  is the current going through the outer probes [48].

All temperature values presented here refer to the chuck temperature as measured using an E-type thermocouple clamped to the side of the chuck. The samples were clamped to the chuck for good thermal contact. The chuck and radiation shield (to which the probes are thermally anchored) are heated using cartridge heaters and a LakeShore 336 temperature controller with a heating rate of 1 K/min. The heated radiation shield reduces the cooling of the sample by the probes; however, due to the large size of the chamber, there is still a significant temperature difference between the chuck and the radiation shield. When the chuck is at the highest temperature,  $\sim 680$  K, the radiation shield is only at  $\sim 420 - 430$  K. Since the distances between the probes are large in these measurements ( $\sim 1$  cm for four-point measurements and  $\sim 1$  mm for two-point measurements) the average film temperature is not expected to be significantly affected by the probes. Resistance versus temperature, from room-temperature up to  $\sim 680$  K for the GST/oxide samples and up to  $\sim 650$  K for the GST/nitride samples, is measured to study the effect of the underlying film on the GST crystallization temperatures.

### 3.3 Scanning Auger Microscopy (SAM) measurements

Auger Electron Spectroscopy (AES) (Figure 3.2) is an analytical technique used specifically in the study of surfaces of the solid materials to determine the elemental composition, the atomic concentration, the depth profile and the chemical state of the atoms.



Figure 3.2. Perkin Elmer PHI 670 Scanning Auger Microscope (SAM).

The AES tool and experimental setup used is part of the Chemistry department at UConn (details in appendix 7.3). Secondary electron detector is used to image the surface of the material and choose the spots for survey analysis. Figure 3.3 shows the map image of the 50 nm GST film on SiO<sub>2</sub> substrate and 3 spots where the full survey spectrum was performed.

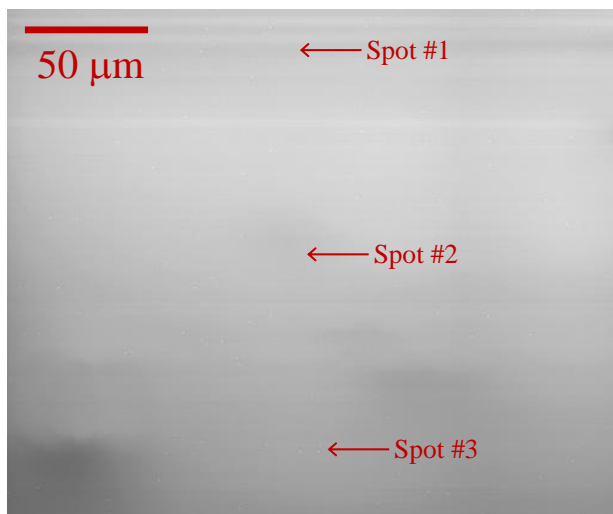


Figure 3.3. Electron detector map image for the 50 nm GST film on SiO<sub>2</sub> substrate.

The full survey spectrum for the 10 nm GST film on SiO<sub>2</sub> substrate is shown in Figure 3.4, along with element concentrations. Any sample exposed to ambient air has C and O on the surface due to adsorption of hydrocarbons and water, and surface oxidation.

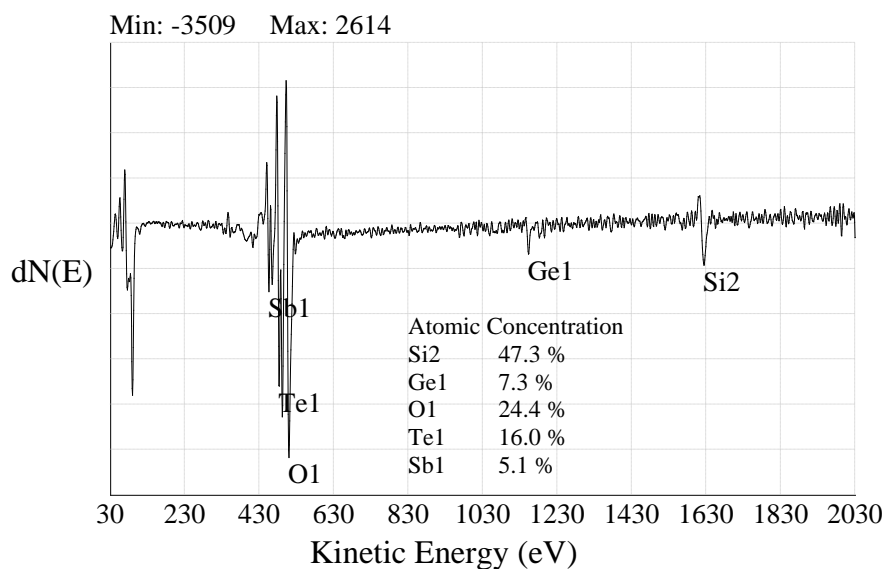


Figure 3.4. The full survey spectrum for the 10 nm GST film on SiO<sub>2</sub> substrate, along with element concentrations.

The Si, Ge, and O profiles do not seem to show sharp interfaces with the surrounding SiO<sub>2</sub> layers. There can be two reasons behind this: (1) diffusion of atoms may erase a sharp interface, or (2) the inherent limit of depth resolution by electron spectroscopic methods has been reached.

The shape of the Si and N profile lines suggest diffusion of atoms across the GeSbTe/ Si<sub>3</sub>N<sub>4</sub> interface, but diffusion may appear larger than actually occurs due to the relatively large probe depth. Atomic concentration as a function of Ar<sup>+</sup> sputter time for 20 nm and 50 nm thick GST films on SiO<sub>2</sub> and Si<sub>3</sub>N<sub>4</sub> are shown in Figure 3.5 and Figure 3.6, respectively.

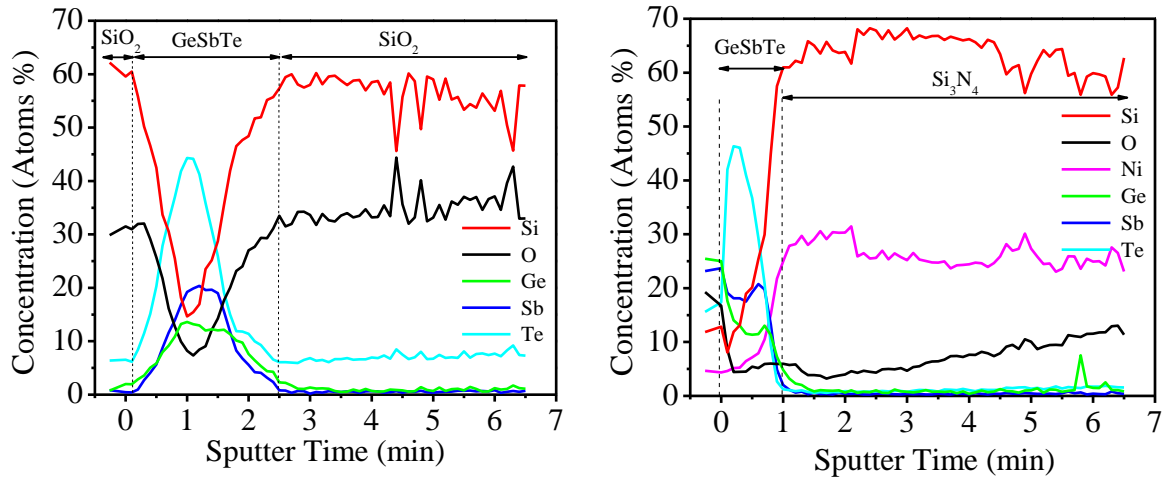


Figure 3.5. Atomic concentration as a function of Ar<sup>+</sup> sputter time for GST films of 20 nm thickness on SiO<sub>2</sub> (left) and on Si<sub>3</sub>N<sub>4</sub> (right).

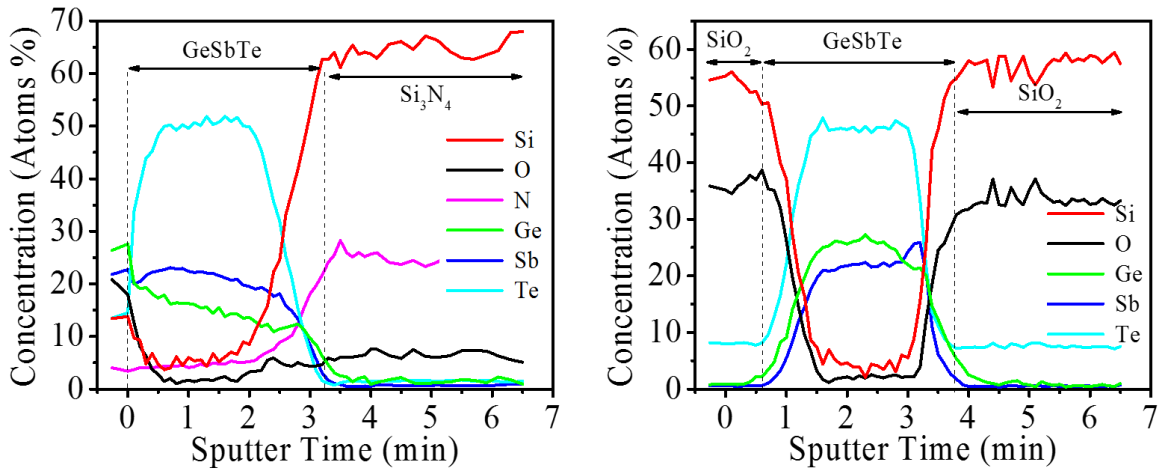


Figure 3.6. Atomic concentration as a function of  $\text{Ar}^+$  sputter time for GST films of 50 nm thickness on  $\text{Si}_3\text{N}_4$  (left) and on  $\text{SiO}_2$  (right).

The thickness of the GeSbTe film does not need to be determined from the depth profile, but the shape of the “breakthrough” section of a profile line may help to assess the effects of diffusion across interfaces. Conversion of the sputter time axis to units of sputter depth is therefore desirable. A common method of choosing sputter times involves fitting sigmoidal curves to the “breakthrough” sections of a profile line. The intersection of the tangent of the curve at its inflection point with an asymptote provides a consistent criterion for choosing values of time.

$$\text{Sputter depth: } D_{\text{Sputter}} = \text{Rate}_{\text{Sputter}} \times \text{Time}_{\text{Total}}.$$

$$\text{Time}_{\text{Total}} = 6.589 \text{ min} - 1.141 \text{ min} = 5.448 \text{ min}.$$

$$\text{Rate}_{\text{Sputter}} = 100 \text{ nm} / 5.448 \text{ min} = 18.36 \text{ nm} / \text{min} = 183.6 \text{ \AA} / \text{min}.$$

The sputter rate is calculated as 18.36 nm/min by using atomic concentration of Sb as a function of sputter time graph (Figure 3.7). Atomic concentration of



elements as a function of film depth is shown in Figure 3.8 for 100 nm GST films on  $\text{SiO}_2$  and  $\text{Si}_3\text{N}_4$ .

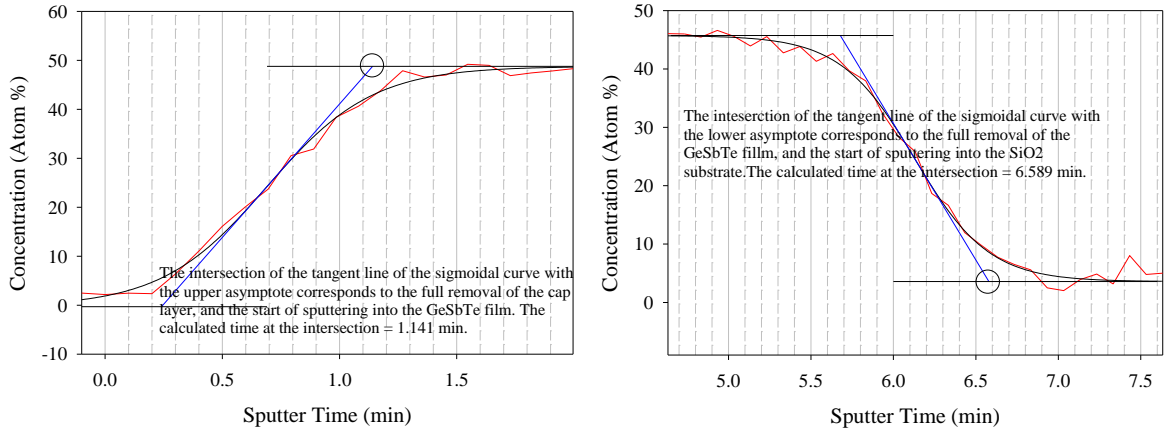


Figure 3.7. Atomic concentration of Sb as a function of  $\text{Ar}^+$  sputter time for 100 nm GST films to show the use of the sigmoidal curve and the asymptotes in determining values of time.

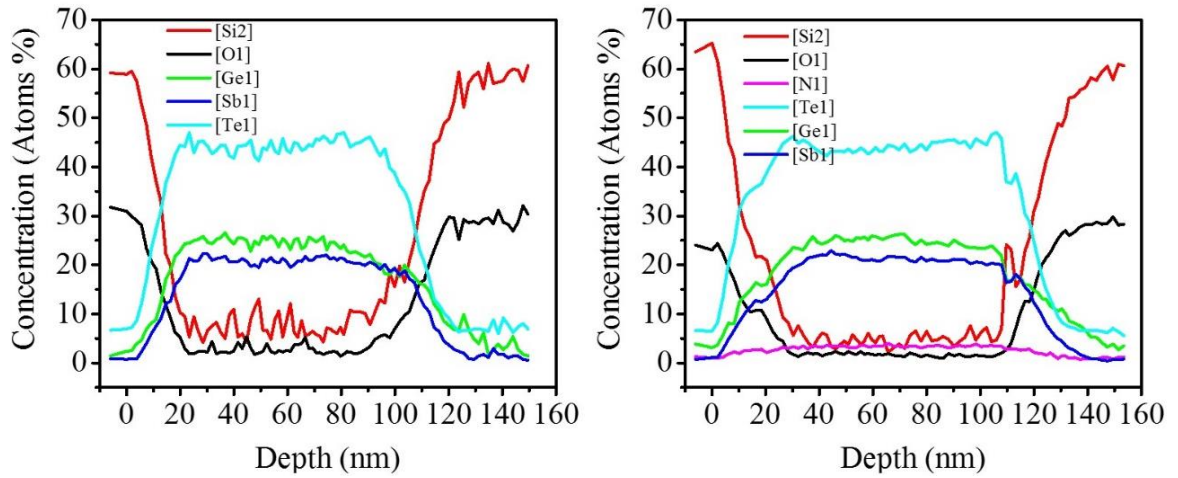


Figure 3.8. Atomic concentration of elements as a function of film depth for GST films of 100 nm thickness on  $\text{SiO}_2$  (left) and on  $\text{Si}_3\text{N}_4$  (right).

### 3.4 Results and Discussion

Figure 3.9 shows the resistivity versus temperature data obtained for GST thin films of various thicknesses on silicon dioxide and silicon nitride. A distinct behavior is observed for the two types of samples. The first phase transition, from amorphous to fcc, is observed at approximately the same temperature for all samples ( $\sim 170$  °C) but the second phase transition, from fcc to hcp, is observed at  $\sim 260$  °C for the GST/nitride samples and at  $\sim 340$  °C for the GST/oxide samples. The fcc-hcp phase transition of GST may be facilitated in the GST/ nitride samples due to the hexagonal symmetry of the underlying silicon nitride [49]. This behavior may also be due to different mechanical stress and adhesion properties for the GST films on silicon nitride and silicon dioxide [50]. It has been reported that crystallized GST films have more stress than amorphous films [51] which could be related to the fact that we observe this substrate dependence for the second transition but not the first. For the 10 nm GST/nitride sample, the second transition is not observed; the resistance starts increasing before the expected second transition, likely due to film segregation into discontinuous regions near the metal pads (observed after the measurements under Scanning Electron Microscopy, Figure 3.10).

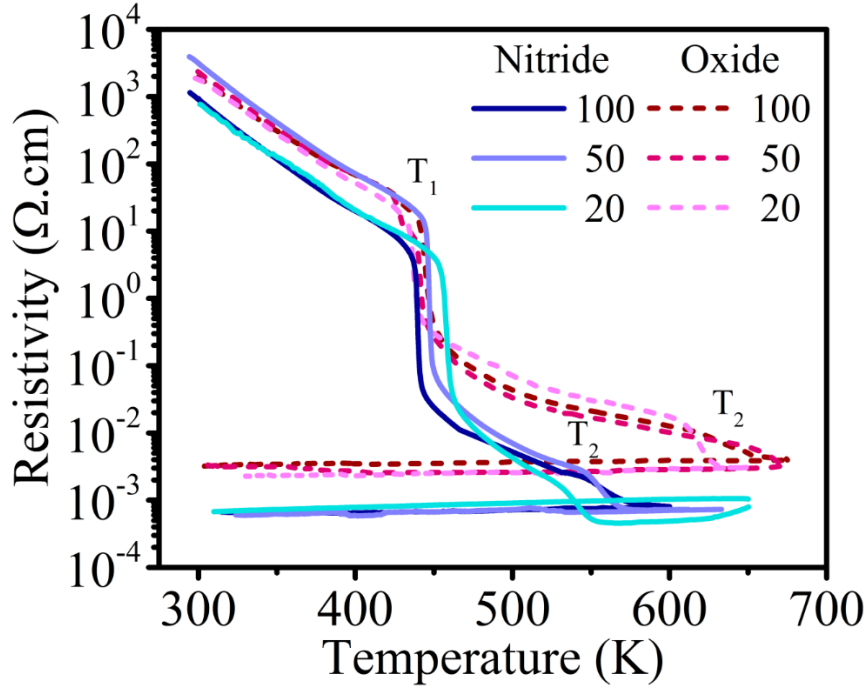


Figure 3.9. Resistivity as a function of temperature for  $\text{Ge}_2\text{Sb}_2\text{Te}_2$  films on silicon nitride and silicon dioxide starting as amorphous (as-fabricated) showing phase transitions from amorphous to fcc and from fcc to hcp at  $T_1$  and  $T_2$  respectively. Resistivity is extracted from resistance measurements using two-point measurement with platinum contacts or four-point measurements using tungsten tips directly probing the GST films. For the thinnest film (10 nm) on silicon nitride the second transition is not observed as the resistance starts increasing before the expected transition temperature, possibly due to film segregation into discontinuous regions.

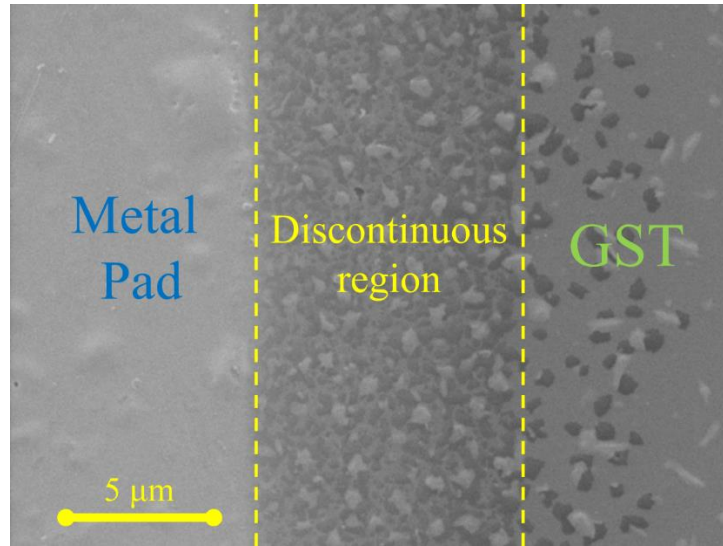


Figure 3.10. Scanning Electron Microscopy image of the 10 nm thick GST/nitride sample after the R-T measurement up to  $\sim 600$  K. The resistance started increasing at  $\sim 540$  K, likely due to the observed segregation of the film into discontinuous regions near the metal pads.

Small variations in resistivity obtained for the different samples are expected from the errors in thicknesses and small differences in contacts shape and separation (for the two-point measurement cases) or probes separation (for the four-point measurements case). The phase transition temperatures  $T_1$  (amorphous-fcc) and  $T_2$  (fcc-hcp) are shown in Figure 3.11 for all samples. These phase transition temperatures are extracted from the R-T measurement as the point at which the first derivative of  $R(T)$  reaches a local minimum, which takes place approximately in the middle point of the transition region.

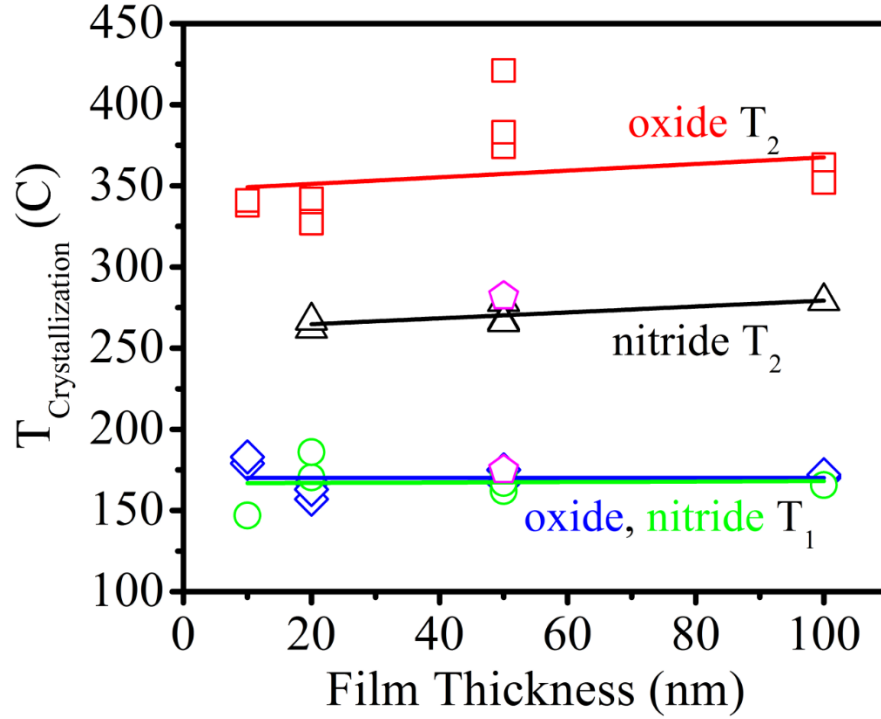


Figure 3.11. GST phase transition temperatures  $T_1$  (amorphous to *fcc*) and  $T_2$  (*fcc* to *hcp*) as a function of film thickness obtained from various measurements on both GST/oxide ( $T_1$   $\diamond$ ,  $T_2$   $\square$ ) and GST/nitride ( $T_1$   $\circ$ ,  $T_2$   $\Delta$ ) samples. For the GST/nitride samples large area contact pads were used for 2-point R-T measurements. For the GST/oxide samples tungsten probe tips were used for 4-point measurements. In all 50 nm GST/oxide samples the GST film was patterned by deposition through a contact mask. One of the 50 nm thick GST/nitride samples ( $\blacklozenge$ ) was measured using tungsten tips to directly probe the GST film (4-point measurement). The 100 nm thick GST/nitride sample was measured with similar size contacts ( $\sim 1 \text{ mm} \times 1 \text{ mm}$ ) formed using graphite paste. The transition temperatures are extracted as the point at which the first derivative reaches the two local minima.

Figure 3.12 shows the room-temperature resistivity for all samples in the amorphous, *fcc* and *hcp* phases. The amorphous samples were deposited as amorphous. The *fcc* and *hcp* samples were deposited as *fcc* or *hcp* (GST/nitride

samples) or heated to temperatures above these phase transitions (GST/oxide samples). All samples have similar resistivities in each phase indicating that the crystalline structures in the GST/nitride and GST/oxide samples are similar and that the as-deposited or crystallized fcc and hcp phases are also similar.

The effect of two different heating rates (1 K/min and 5 K/min) on the R-T characteristics was found to be significant (Figure 3.13). The phase transitions are observed at slightly lower temperatures for the slower heating rate (for both GST/nitride and GST/oxide samples). For the GST/nitride samples, the transition temperatures appear to increase with increasing film thickness, with a more marked trend for the faster heating rate [52].

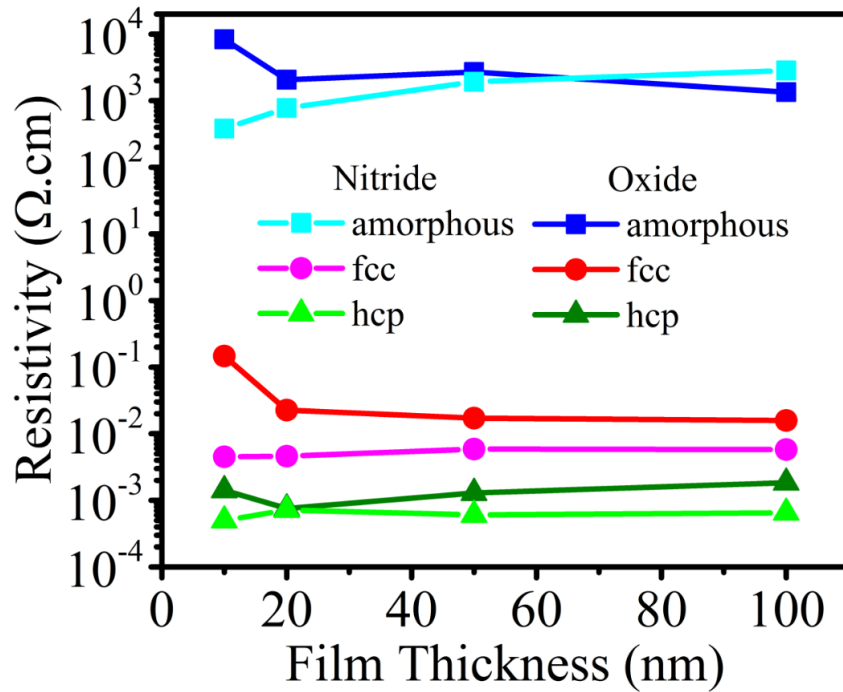


Figure 3.12. Room temperature resistivity for all thickness films on GST/nitride and GST/oxide samples, in amorphous, cubic and hexagonal phases. The fcc and hcp GST films on GST/oxide sample are obtained by heating as-deposited

amorphous films to 565 K or 670 K (above the first or second transition) followed by cooling to room temperature for resistivity measurements. GST films on GST/nitride samples are deposited as amorphous, fcc or hcp.

Figure 3.11 shows that, for films from  $\sim 10$  to  $\sim 100$  nm thickness, the first transition temperature did not depend on the film thickness but the second transition temperature increased as the film thickness increased. These earlier measurements had been performed in  $N_2$  atmosphere using an inductive heating setup, with an average heating rate of  $\sim 3$  K/min from room temperature to the maximum temperature of  $\sim 330$  °C (no temperature controller) and the sample temperature was measured by a K-type thermocouple clamped to the sample surface [47]. While there still appears to be a small thickness dependence effect on the transition temperatures of the GST films on silicon nitride using a slow heating rate (1 K/min) (Figure 3.13) the current data shows that the heating rate has a more significant effect on the observed transition temperatures. This could be due to the difference between the measured chuck temperature and the actual film temperature; however, the large chuck, samples, and separation between the probe tips suggest the observed transition temperature variations with heating rate and thickness (especially for the faster heating rate) are more likely due to the finite crystallization times of the material at a given temperature.

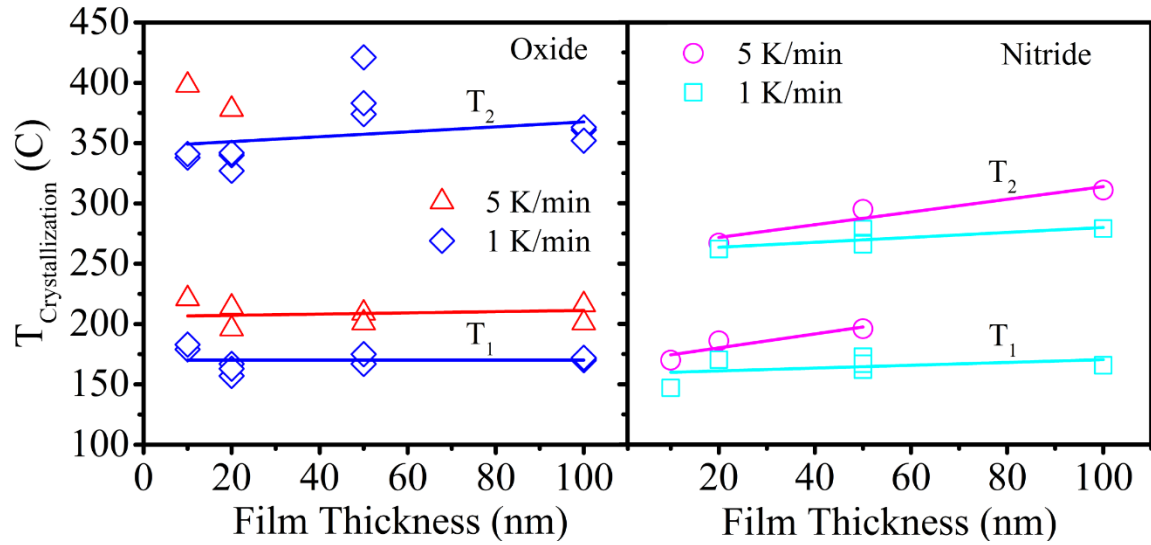


Figure 3.13. Phase transition temperatures observed from resistance versus temperature measurements (R-T) with heating rates of 1 K/min and 5 K/min on GST films of various thicknesses on GST/oxide (left) and GST/nitride (right) samples.

If the crystallization times are slow compared to the heating rate, the structure does not have time to re-arrange itself before the resistance is measured and the transition will appear to happen at a higher temperature. For the thicker GST/oxide samples heated at 5 K/min (50 and 100 nm), the fcc-hcp phase transition is not observed, presumably because it occurs at a temperature higher than can be reached with the setup ( $\sim 400$  °C) or because it is slow compared to the heating rate.



## **4. The Effect of a Baseline Voltage on Crystallization of Nanoscale Ge<sub>2</sub>Sb<sub>2</sub>Te<sub>5</sub> Devices**

The crystallization time scale of Ge<sub>2</sub>Sb<sub>2</sub>Te<sub>5</sub> ranges from > 10 years at room temperature [53] to ~100 ns close to melting temperature ( $T_{melt-GST} \sim 900$  K) [11, 38, 54-59] with maximum growth velocity of ~1 m/s [60].

Recent reports of very fast crystallization in pore PCM structures (< 1 ns) upon melting with a low voltage baseline before and after the melting pulse attribute this accelerated crystallization to the formation of a pre-nucleated state by the baseline voltage (after the pulse) [61].

We have combined detailed electrical measurements with finite element modeling to understand the effect of different baseline voltages on the crystallization of GST line structures after melting pulses and possible origins for the apparent very fast crystallization.

### **4.1 Constant Baseline Voltage Before and After Melting**

#### **4.1.1 Experiments on GST Line Cells**

A baseline voltage is applied before and after a melting reset pulse to control and monitor the crystallization dynamics, as shown in Figure 4.1. Experimented GST line cell structures with bottom metal contacts were fabricated using conventional photolithography and semiconductor processing techniques on bulk Si wafers. Detailed fabrication processes described in section 2.2. The resulting device dimensions were measured by Scanning Electron Microscope (SEM) (Figure 4.3 b).

The baseline electrical measurements were performed by melting the wires via

self-heating by applying a short voltage pulse with varying baseline voltage amplitudes before and after the pulse (Figure 4.1 a). An Agilent 8114A pulse generator (PGU) and a Tektronix TDS 724D oscilloscope were configured as shown in Figure 4.1 a inset for the measurements, using short coaxial cables for connections. Several load resistors are used to limit the current during the pulse to prevent damage of the device breakage. Load resistors were provided by either mounting them on micro-manipulator probe arms (leading to additional 10 pf capacitance) or by a surface-mount resistor attached to the probe tips (Figure 4.1 b inset) (without any additional capacitance). 2 to 3 V pulses with 100 ns durations and varying baseline offset were applied to fully melt GST wires of varying sizes.

Complete melting of the structures is observed as a plateau in the current during the pulse (Figure 4.1 b), as observed earlier for silicon microwires [36]. The shapes of the electrical current versus time characteristics (Figure 4.1 b) suggest that after the melting pulse, the GST wires may stay partially molten (due to retention of a current carrying filament) and recrystallize in a growth-from-melt manner, or they may resolidify immediately as amorphous depending on the applied baseline voltage (Figure 4.2 ). A liquid filament region has enough heat capacity to crystallize the surrounding solidified region after the main pulse. The baseline voltage is used to measure the wire resistance before and after the pulse to determine the phase of the material.

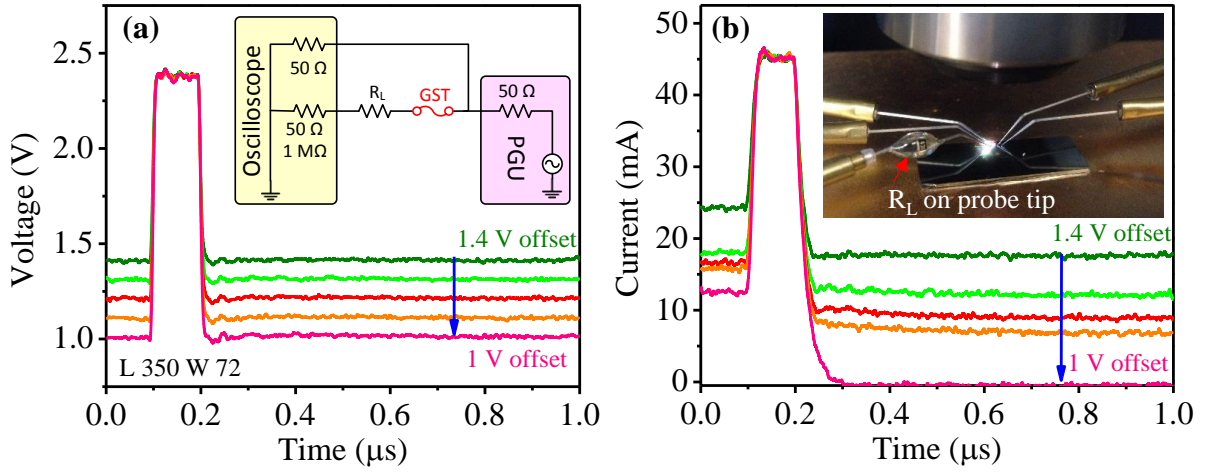


Figure 4.1. Applied voltage pulses (a) and measured current (b) with offset voltages varying from 1.4 V to 1 V on a Length: 350 nm Width: 72 nm device. Circuit schematic of the experimental setup (inset a) and load resistors attached on probe tips (inset b).

Figure 4.1 a shows example data for 2.4 V 100 ns pulses with different offset voltages (from 1.4 V to 1 V). For this particular device (Length: 350 nm Width: 72 nm) offset voltage amplitudes above 1.1 V are enough to result in recrystallization of the wire after melting as seen by the large increase in current. Lower baseline amplitudes, however, cannot keep the amorphous volume hot enough upon re-solidification and lead to amorphization of the device.

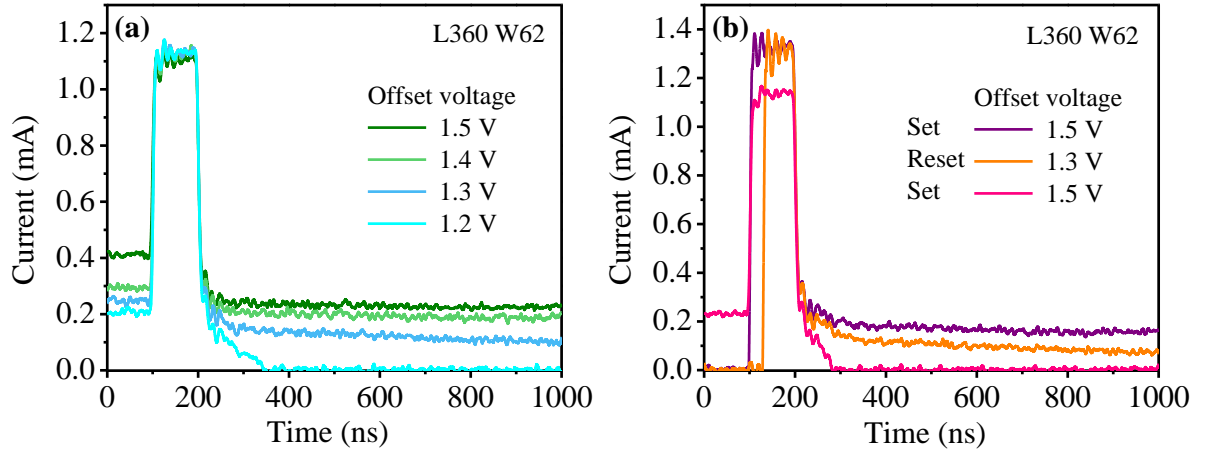


Figure 4.2. Measured current signals on a GST wire with varying offset voltages (1.5 V to 1.2 V) (a), with different offset voltages (b) to show the effect of offset voltage by switching between amorphous and crystalline phases.

Figure 4.2 shows measured current signals on a GST wire (L: 360 nm W: 62 nm) for 100 ns pulses with varying offset voltages amplitudes. Maximum applied voltage is kept at 4V for all cases while varying the baseline amplitude. Above 1.2 V offset voltage, the material re-crystallizes after re-solidification ( $R_{\text{wire}} = 5.7 \text{ k}\Omega$ ) via liquid filament retention. For 1.2 V offset voltage, the current decreases as the solid amorphous material cools down and the wire remains amorphous ( $R_{\text{wire}} = 26.6 \text{ M}\Omega$ ). After the wire is amorphized ( $R_{\text{wire}} = 26.6 \text{ M}\Omega$ ) due to the low offset voltage, a new pulse is applied with a higher offset amplitude (3V + 1.5 V offset) and the wire recrystallizes ( $R_{\text{wire}} = 3.3 \text{ k}\Omega$ ). This process is then repeated ( $3.3 \text{ k}\Omega \rightarrow 94 \text{ M}\Omega \rightarrow 3.47 \text{ k}\Omega$ ) to show that the same melting pulse followed by smaller or larger baseline voltage can be used to repeatedly amorphize or crystallize the structure (Figure 4.2 b).

### 4.1.2 Simulations of GST Line Cells

Unlike conventional electronic devices, PCM utilizes heating to crystallize (set), and melting and resolidification to amorphize (reset). Hence, the material in the active region changes dynamically along with the thermal profiles. Many different models have been proposed to model the changes in the material during operation and the resulting device behavior. First, compact models have been proposed to construct SPICE models of PCM devices and optimize cell geometries [62-65]. These compact models however rely on many assumptions including device symmetry, and do not account for stochastic nucleation or filament formation. These models also do not calculate local phase distributions within devices during their operation. To model the phase change properties of the material, many Arrhenius (JMAK) models have been proposed [66, 67]. These models use Arrhenius approximations for the crystal fraction as a function of time in PCM devices. In our laboratory electrothermal models have been used to model both set and reset operations of PCM devices, including temperature dependent physical parameters of the materials and thermoelectric effects [16, 32, 68, 69]. In order to capture the nucleation, growth and amorphization processes during the simulations, these models have evolved to include a local crystal density function (CD) which is tracked using a rate equation and where  $CD = 0$  and  $CD = 1$  correspond to fully amorphous and fully crystalline volumes.[70] This crystal density model includes crystalline nucleation rate and growth velocity of the material from the literature.

GST line cell structure (Figure 4.3) is simulated using COMSOL Multiphysics finite element simulations with 2-D rotational geometry. The device dimensions and

series load resistor ( $3\text{k}\Omega$ ) are chosen to get a similar GST volume with our experimental GST line cell structures.

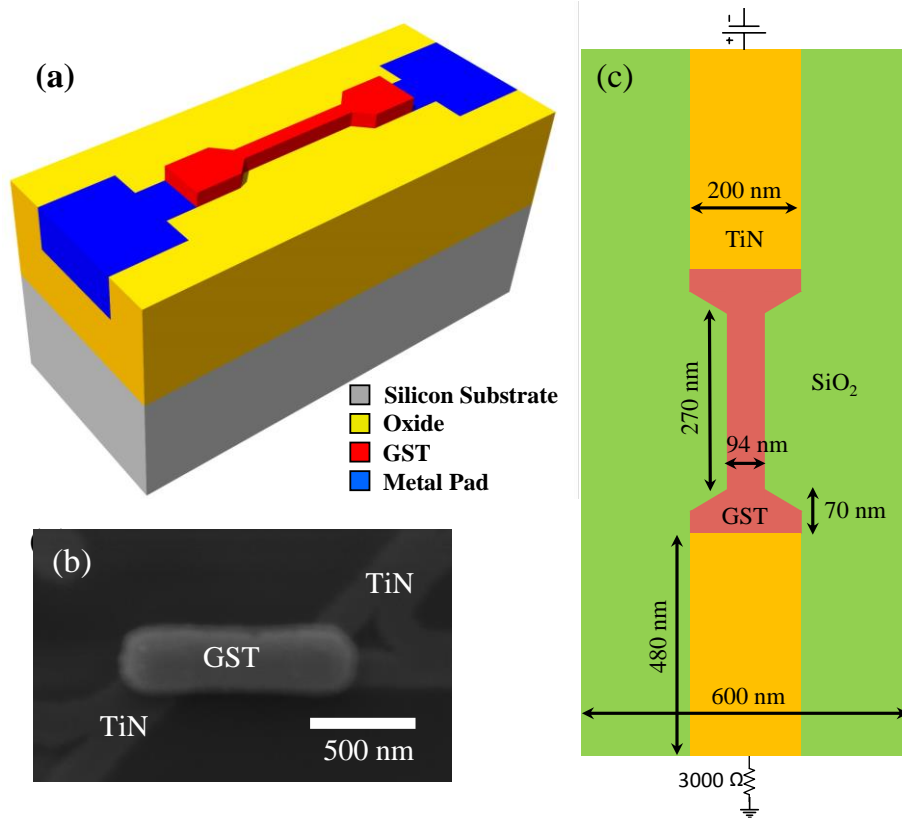


Figure 4.3. Schematics of a fabricated line cell structure with contact pads (a). SEM image of a fabricated line cell (b) Cross section of the simulated line cell geometry and materials (c).

10 V 100 ns main pulse with varying offset voltages are applied  $1\mu\text{s}$  long to observe the change of current after the main pulse. The large output currents are indicate that the GST is molten with main pulse and depend on the offset voltage amplitude, line cell is crystallized (4.5 V to 2.05 V) or amorphized (under 2 V) (Figure 4.4 a). Figure 4.4 b shows that GST line cell resistances, where low offset voltage applied, increase over

time due to fast quenching (amorphous phase). The line cells which are subjected to higher offset voltage, show lower resistances due to crystallization of the line cells after main pulse.

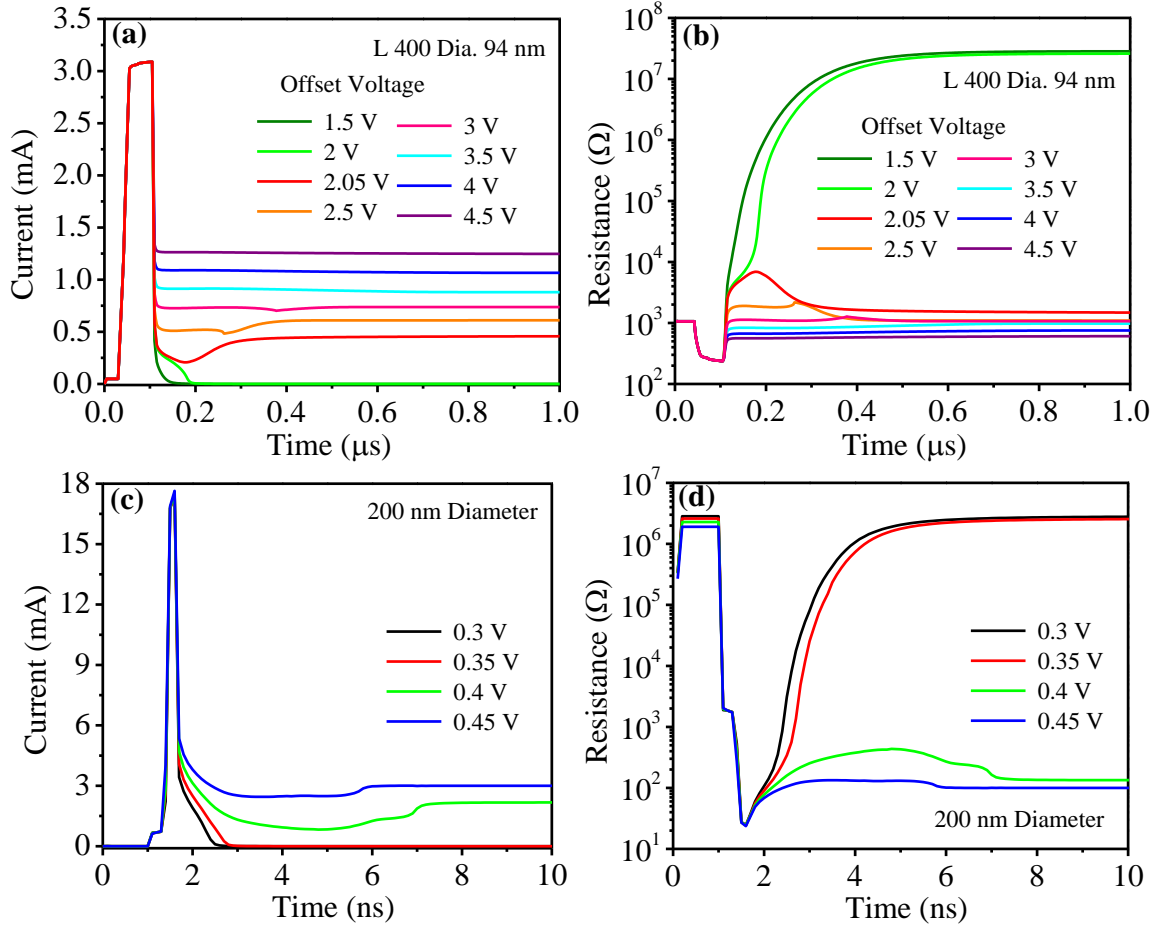


Figure 4.4. Output currents (a), and calculated resistances (b) with varying baseline voltages on simulated (Length 400 nm, Diameter 94 nm) GST line cell. Output currents (c), and calculated resistances (d) with varying baseline voltages on simulated (30 nm thick, Diameter 200 nm) GST pore-like structure.

### 4.1.3 Simulations of GST Pore-like Cells

Pore-like structure PCM cells with  $\text{Ge}_2\text{Sb}_2\text{Te}_5$  as the phase-change material are simulated using COMSOL Multiphysics finite element tool with 2D rotational symmetry, to compare to previously reported experimental results [61]. The GST cells consist of top and bottom TiN contacts with diameter (d) x height (h) = 250 nm x 200 nm, a GST disk in center (height = 30 nm) with varying diameters (d = 25, 50, 100, and 150 nm) and  $\text{SiO}_2$  as the surrounding material. This geometry and dimensions were chosen to match the reported experimental devices [61].

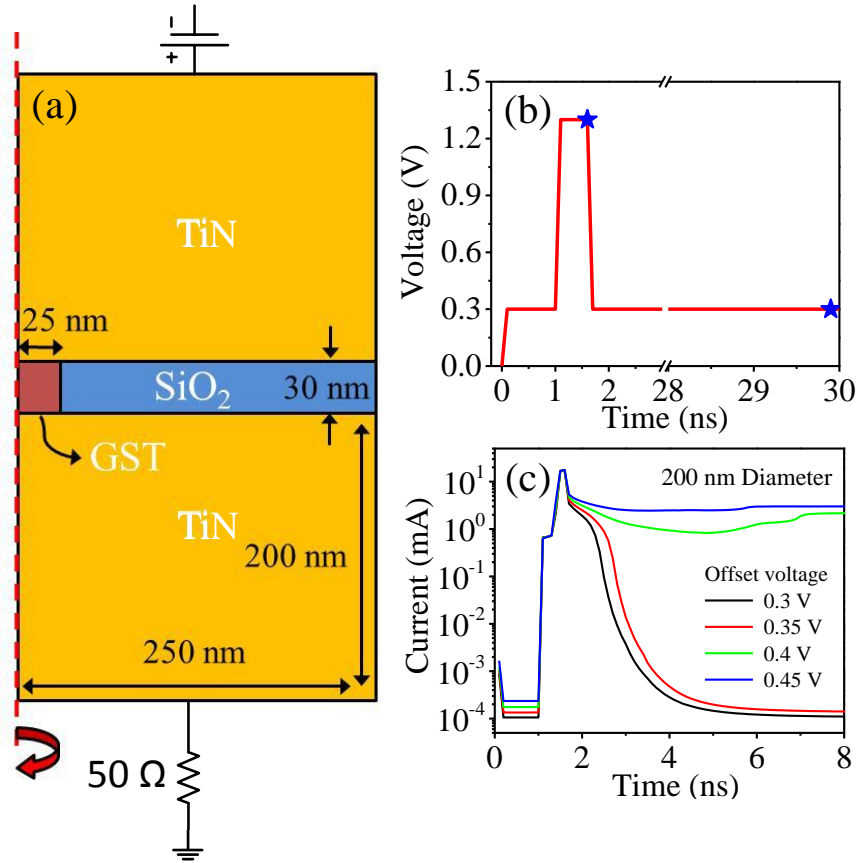


Figure 4.5. Schematic of the simulated pore-like structure PCM cell (a). Applied voltage as a function of time (★ are indicate at the end of the main pulse and at the end of the simulation) (b). Measured current through the GST cell (c).



Figure 4.5 a shows the geometry of the simulated GST pore-like cell. PCM cells simulated by applying 1.3V, 500 ps main pulse with 100 ps rise/fall times on varying baseline voltages (0.3 V- 0.45 V) for a total simulation period of 30 ns.

The large output currents indicate that the GST is molten with the main pulse and depending on the offset voltage amplitude, the line cell is crystallized (0.45 V and 0.4 V) or re-solidifies and remains amorphous (under 0.35 V). Figure 4.5 c shows that with low offset voltages the GST line cell resistance increases over time due to fast quenching (amorphous phase). With higher offset voltages the line cells show lower resistances due to crystallization after the main pulse.

Figure 4.6 shows the temperature profiles of the simulated GST structure (200 nm diameter) with 4 different offset voltage amplitude, at the end of the main pulse and at the end of the simulation (indicated with stars in Figure 4.5 b). White contour lines denote the regions which have reached melting ( $>873$  K). During the pulse and due to the cylindrical shape of the structure the current is confined to an outer region creating a molten ring within the GST. After the pulse, and with large baseline voltages, the molten region shifts and stabilizes at the center of the device due to the surrounding  $\text{SiO}_2$ . Low baseline voltages are not sufficient to keep the region molten and it re-solidifies in amorphous phase.

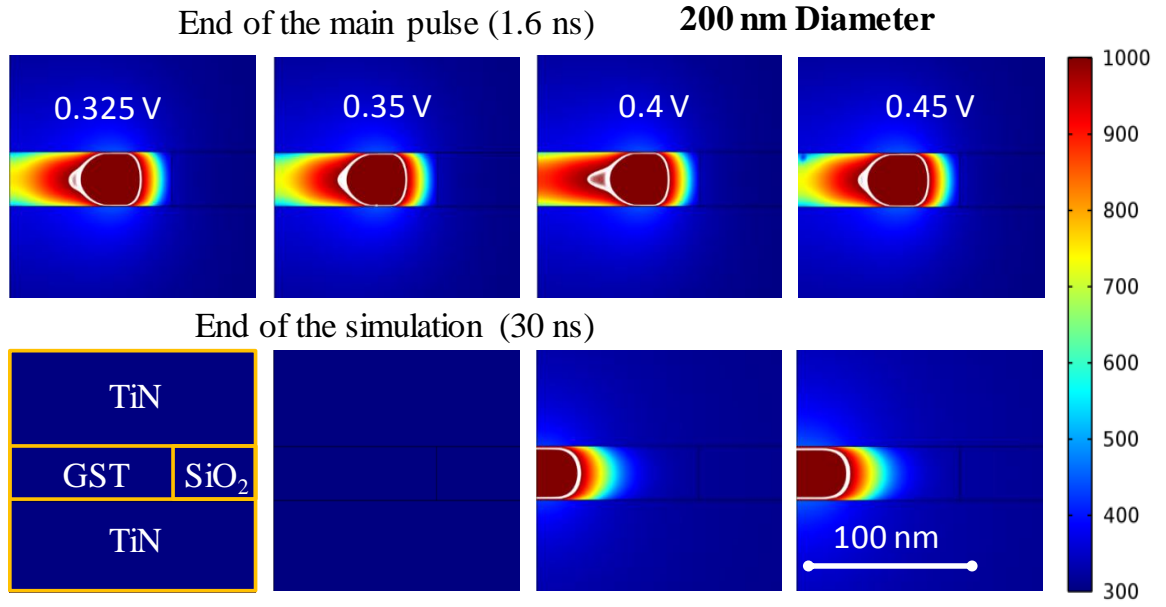


Figure 4.6. Temperature profile of the simulated pore-like structure PCM cell (200 nm diameter GST) using the four different baseline voltages (Figure 1c). Images are captured at the end of the main pulse and at the end of the simulation (indicated in Figure 1b).

The maximum temperature reached as a function of baseline voltage, at the end of the main pulse, is shown in Figure 4.7 for two different GST thicknesses (30 and 50 nm). Some part of the GST element stays molten with lower baseline voltages ( $>325$  mV) for narrower devices (50, 100 nm diameter). Wider structures (200, 300 nm diameter) require higher baseline voltage amplitude ( $> 400$  mV) to retain a molten region due to higher volume and heat diffusion, compared to narrower structures.

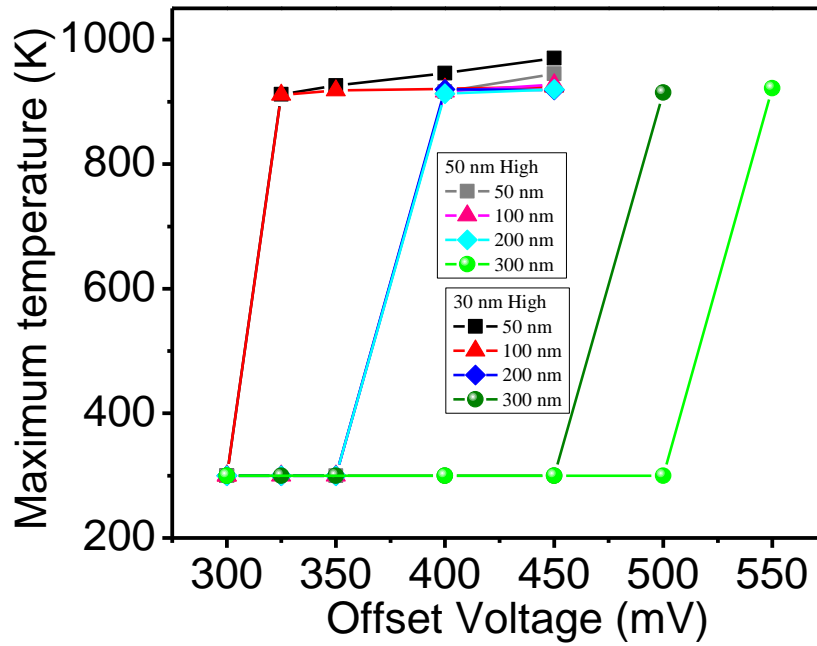


Figure 4.7. The maximum temperature reached as a function of offset voltage at the end of the simulation (30 ns).

The simulated current through the 30 nm thick GST structure is shown in Figure 4.8 for 4 different diameters and 5 different offset voltage amplitudes. The main pulse partially melts the GST structure (or fully melts it, for the 50 nm diameter structure) depending on the following applied baseline voltage amplitude; the structure then re-solidifies as amorphous or recrystallizes (in fcc phase) due to the retained molten region of GST, again depending on the baseline amplitude which determines the extent and duration of the retained molten filament. The maximum temperatures reached within the GST cells as a function of time, for different baseline values are shown in Figure 4.9. Like for the wider and narrower devices, the longer devices re-solidify faster than the shorter devices due to faster heat diffusion and larger volumes.

When the baseline voltage increases the GST element stays at high temperature for a longer period and the re-solidification process is slower due to the higher current.

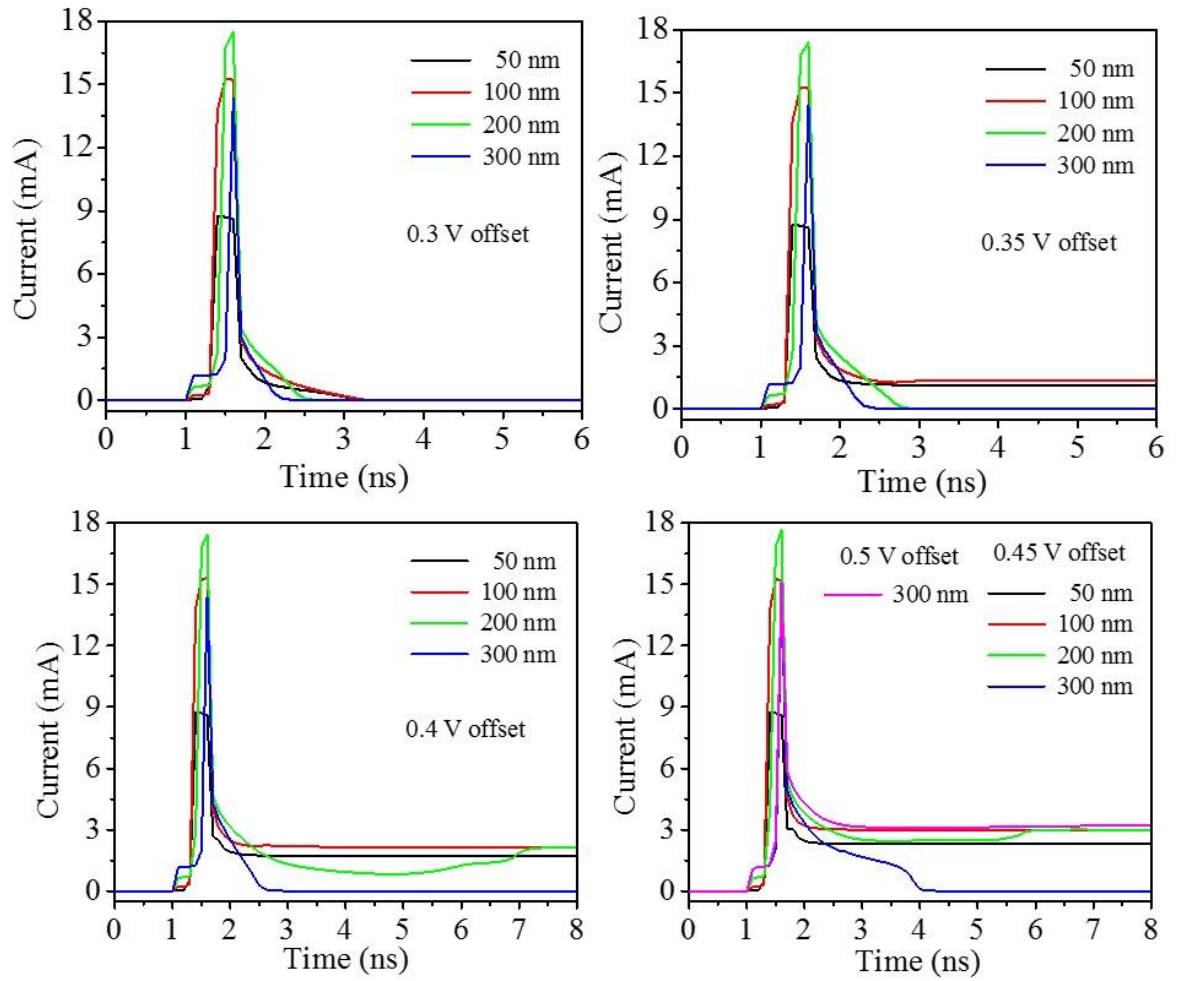


Figure 4.8. Simulated current through various diameters GST cells (height of 30 nm) for different baseline voltages.

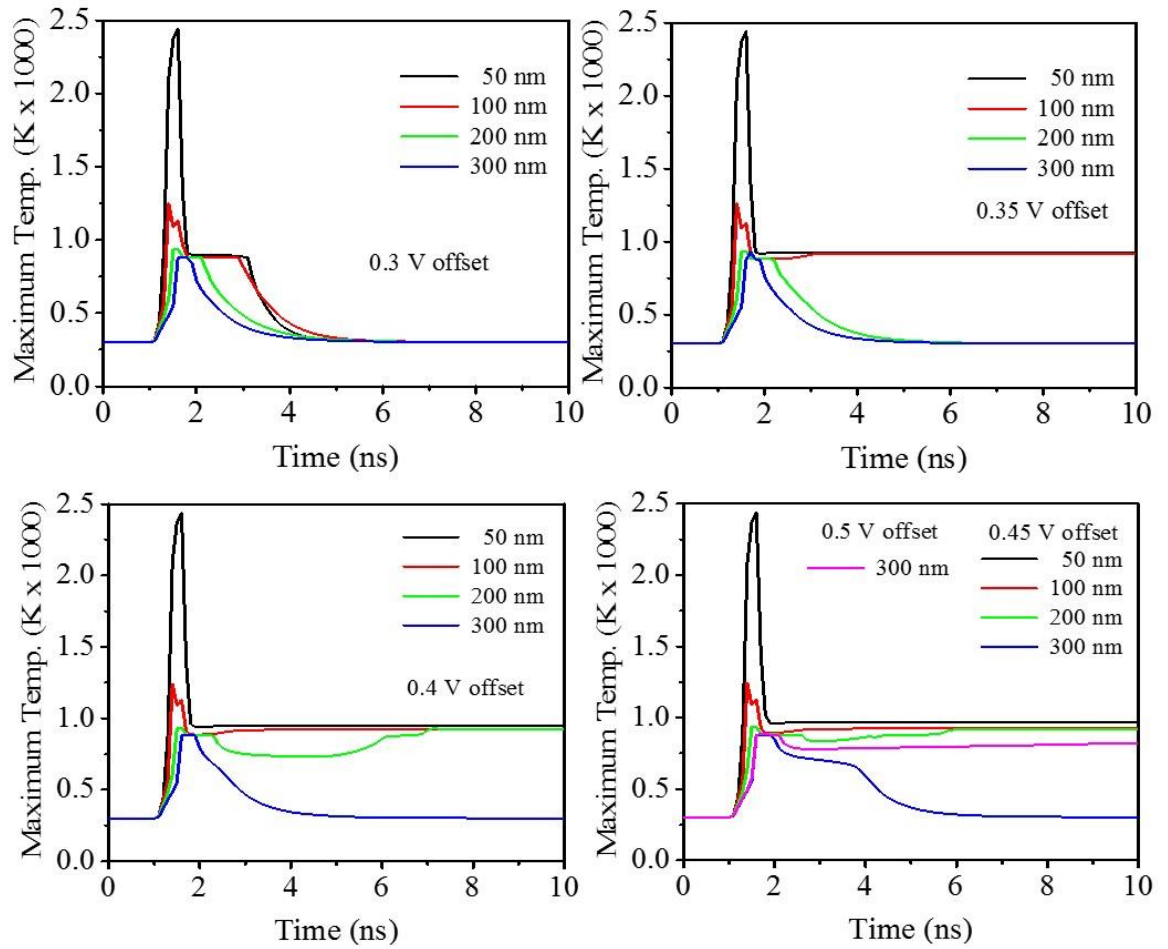


Figure 4.9. Maximum temperature reached within different diameter GST cells for different baseline voltages as a function of simulation time.

## 4.2 Decreasing Baseline Voltage after Melting

### 4.2.1 Experiments on GST Line Cells

GST line cells were annealed at 670 K before the pulse measurements; therefore all of the cells were initially crystalline (hcp phase). A Tektronix AFG 3102 arbitrary function generator was used to create a 3 step 500 ns long main pulse (3 - 4V), followed by a decreasing multistep offset voltage (1.5 to 1.1 V) for a total 20 ms

waveform. A  $3\text{k}\Omega$  surface-mount resistor was attached to one of the probe tips as a load resistor to prevent wire breakage caused by high current during the liquid phase. Applied voltage and output current were captured by a Tektronix DPO 4104 oscilloscope and the wire resistance was obtained from the corresponding data, after subtraction of the load resistance from the total resistance (Figure 4.10). During the melting pulse the output current exceeds the oscilloscope acquisition scale settings and is cropped (Figure 4.10 inset). After the main pulse, the wire becomes molten via self-heating and due to the large starting applied baseline voltage a liquid filament is retained. The following decrease in the baseline voltage causes a reduction in the liquid filament diameter until it completely solidifies. During solidification ( $\sim 1.155\text{ V}$ ), the wire resistance suddenly increases (due to the mixed phase upon fast solidification) before the wire completely crystallizes and the resistance decreases again. After the measurement, the wire resistance was measured by the PA as  $5.711\text{ k}\Omega$  indicating the element crystallized into *fcc* phase.

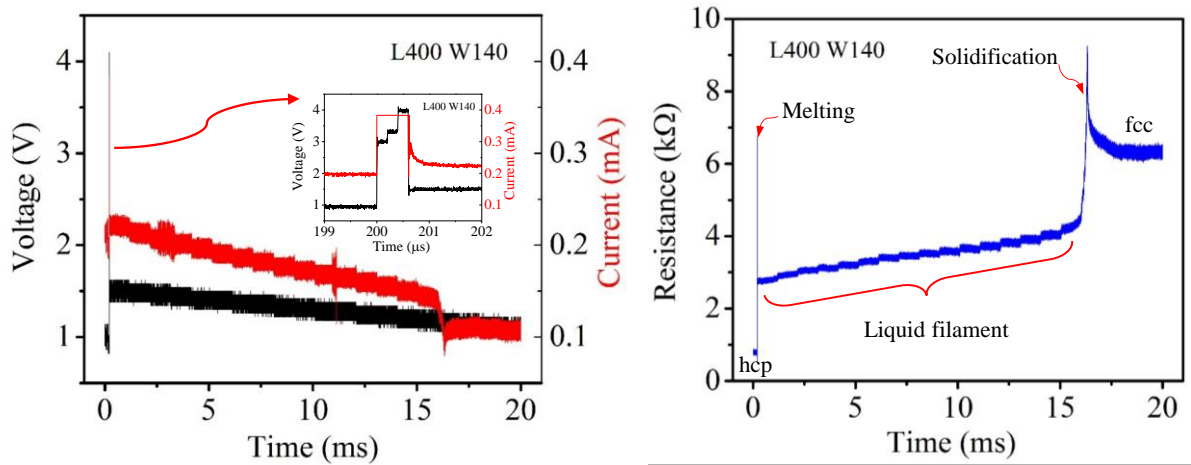


Figure 4.10. Applied voltage and output current (as shown in the measurement setup in Figure 4.1 a inset), and calculated resistance of the GST line cell (Length 400 Width 140 nm and thickness 50 nm).

#### 4.2.2 Simulations on GST Line Cells

To compare to the experimental results on decreasing baseline voltages after melting pulses on a GST line cell, COMSOL Multiphysics [71] finite element simulations of similar waveforms on a GST line with 2-D rotational geometry were performed (Figure 4.11 a, b). 2D rotational symmetry is used for practical computational times. The simulated PCM cell consists of top and bottom TiN contacts with diameter ( $d$ ) x height ( $h$ ) = 150 nm x 500 nm, a GST wire in between of width 50 nm and length 360 nm, and SiO<sub>2</sub> as the surrounding isolation material. Cross section schematics of the simulated wire geometry and materials are shown in Figure 4.11 a including the simulated 500  $\Omega$  series resistor. A 3D sliced view of the simulated line cell is shown Figure 4.11 b.

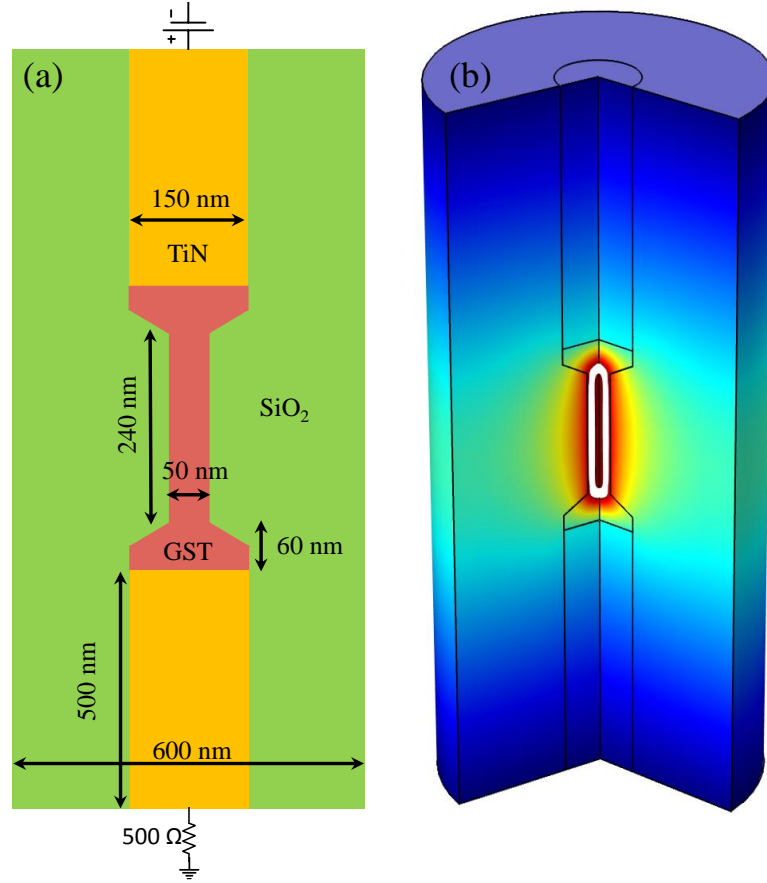


Figure 4.11. Cross section of the simulated line cell geometry and materials. A resistor is added in series to limit the current (a). 3D sliced view of the simulated cell (b).

A 1.7 V, 50 ns main pulse with a 25 ns rise and 10 ns fall time followed by multi-step baseline voltages (from 1.30 V to 1.22 V) is applied to GST line cell (Figure 4.12). The resulting temperature and crystalline density (CD) maps of the simulated cell are shown in Figure 4.13 with corresponding simulation times. The wire is fully molten by the short voltage pulse and the current increases due to the decrease of the resistance. After the main pulse, and during the fall time, a liquid filament is retained, and it starts to shrink down as the applied baseline voltage decreases until it completely re-solidifies at a baseline voltage of 1.21V and crystallizes into *fcc* phase. While the liquid filament shrinks down it gradually crystallizes the surrounding area due to the high temperature



and heat capacity of the liquid region. During the solidification of the liquid filament, the current decreases abruptly due to the significant resistivity difference between the liquid and crystalline phases. The applied voltage waveform and resulting current and resistance as a function of simulation time are shown in Figure 4.12.

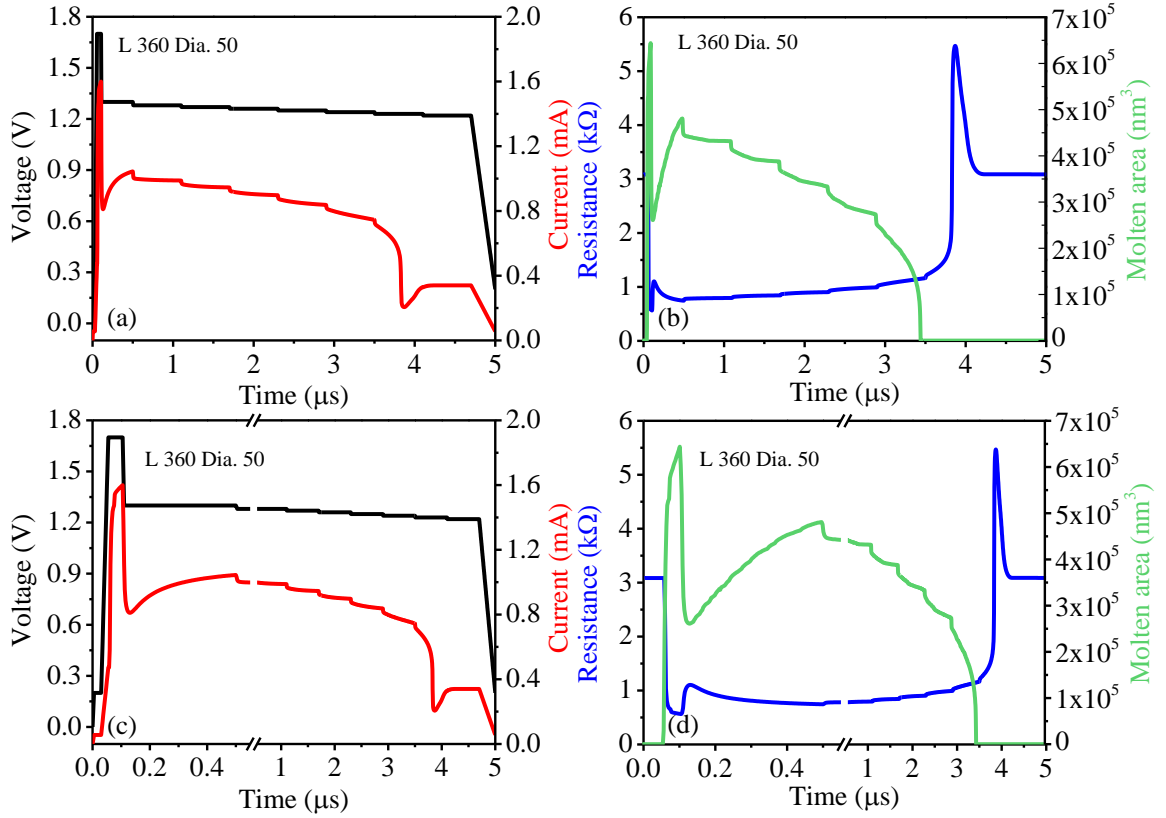


Figure 4.12 Simulated applied voltage waveform and output current (a) and resistance and molten volume (b) of the simulated GST line cell (length 360 nm, diameter 50 nm). (c) and (d) show a ‘zoomed-in’ view of the same data in the period after the melting pulse.

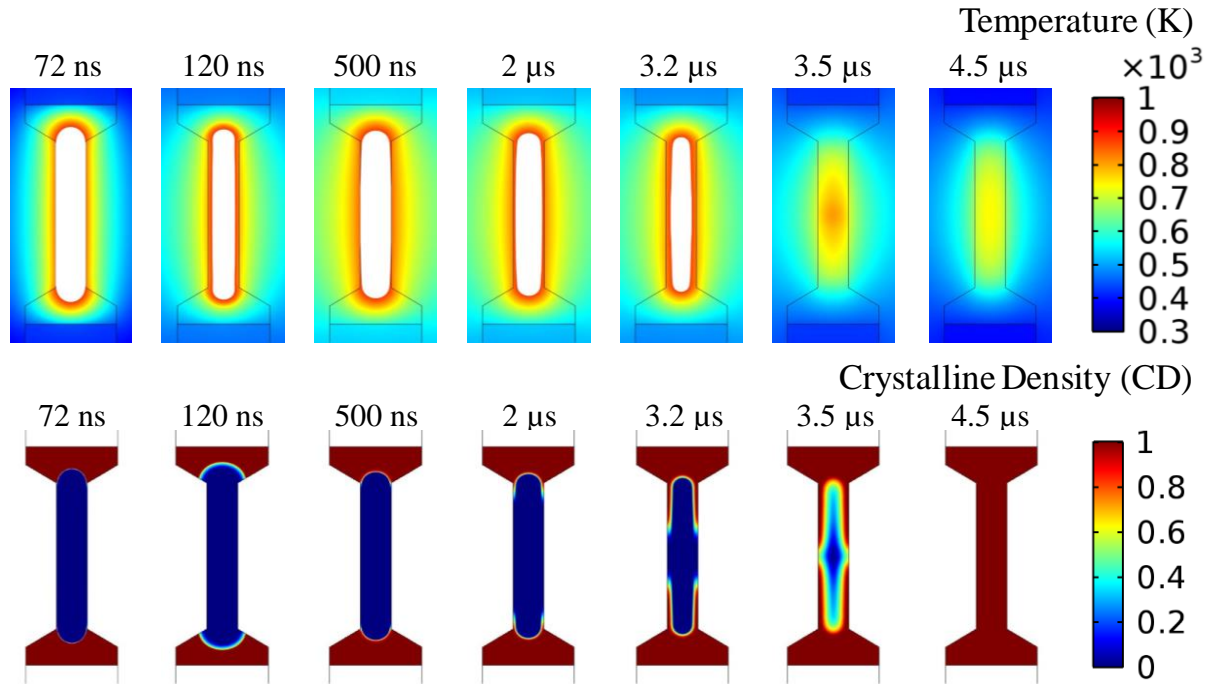


Figure 4.13. Temperature and crystalline density profiles of the GST wire during the simulation, at given simulation times. The white areas indicate the molten regions ( $T > 873$  K).

The simulations show the same general behavior of the current and resistance of the cell with decreasing baseline voltages after a melting pulse, in agreement with the interpretation of the experimental data in terms of a liquid filament that remains after the melting pulse and leads to crystallization of the surrounding region as it shrinks down.

### 4.3 Summary

Experiments and simulations show that after a melting pulse, the GST structures can stay partially molten through the retention of a current carrying filament, re-solidify as amorphous and crystallize over time, or re-solidify as amorphous and remain amorphous, depending on the baseline voltage amplitude that follows the melting pulse.

These results suggest that in previous reports of ultra-fast crystallization of GST pore-like cells melted with a  $\sim 500$  ps pulse followed by a baseline voltage, the crystallization process may have happened after the pulse and because of the baseline voltage that allowed for re-crystallization [61]. Monitoring the current through the structure is necessary to understand the phase of the material after the melting pulse.

## **5. *In-situ* and *ex-situ* XRD measurements of GeSbTe thin films at various annealing temperatures**

### **5.1 Introduction**

X-ray diffraction measurements were performed on GST thin film samples to determine the grain sizes with increasing annealing and measurement temperature. Two types of measurements were conducted, both starting from as-deposited amorphous GST samples: 1) *in-situ* annealing with XRD scanning taken during ramping after stabilization at each target temperature; and 2) annealing at a target temperature (one temperature ramp from room temperature to final target temperature at which the sample is annealed for 15 minutes, on a different hot chuck) followed by room temperature XRD measurements (*ex-situ*).

### **5.2 XRD Measurements**

The samples used for these experiments were ~ 200 nm thick GST films deposited on ~ 600 nm SiO<sub>2</sub> on single-crystal silicon wafers by co-sputtering deposition. The GST films were encapsulated with 10 nm Si<sub>3</sub>N<sub>4</sub> to prevent oxidation and evaporation of the films.

A Bruker D8 Advance x-ray diffraction with nickel coated high vacuum oven chamber system was used for the *in-situ* XRD measurements. The system allows changing the incident beam slits to control the height and width of the incident X-ray spot. 1 mm and 8 mm slits were used for the X-ray source and detector respectively.

For the *in-situ* measurements, the samples were annealed from room temperature to a final temperature in target step temperatures on a hot chuck in the

XRD system oven chamber. After the chuck stabilizes at each target temperature the X-ray scanning was performed with scanning angle ( $2\theta$ ) from 20 to 55 degrees which takes approximately 34 minutes to complete.

After gathering X-ray intensity data as a function of Bragg angle, background noise is eliminated by using analysis software. Average grain size is calculated using the Scherrer equation (Eq. (5.1) ) where  $L$  is average grain size [72],  $K$  is the dimensionless shape factor ( $\sim 0.9-1$ ),  $\lambda$  is the X-ray wavelength and  $\beta$  is the line broadening at half the maximum intensity (FWHM) in radians.

$$L = \frac{K\lambda}{\beta \cos \theta} \quad (5.1)$$

Figure 5.1 shows an example x-ray intensity peak of GST thin film at 300 °C and in-situ XRD patterns of GST thin film at various chuck temperatures. The initial GST thin film is as amorphous and until 175 °C there is no intensity peak. When the chuck temperature increases, with 2°C/min heating rate, GST starts to crystallize into *fcc* with corresponding intensity peaks. The small widening of the intensity peaks as the temperature increases is caused by an increase in grain size due to temperature dependent nucleation and growth [73]. When the chuck temperature reaches 300 °C the material switches from *fcc* phase to *hcp* phase. By increasing the chuck temperature to higher

temperatures the X-ray peak's width and maximum intensity continue to increase which shows increasing crystalline grain sizes up to melting temperature.

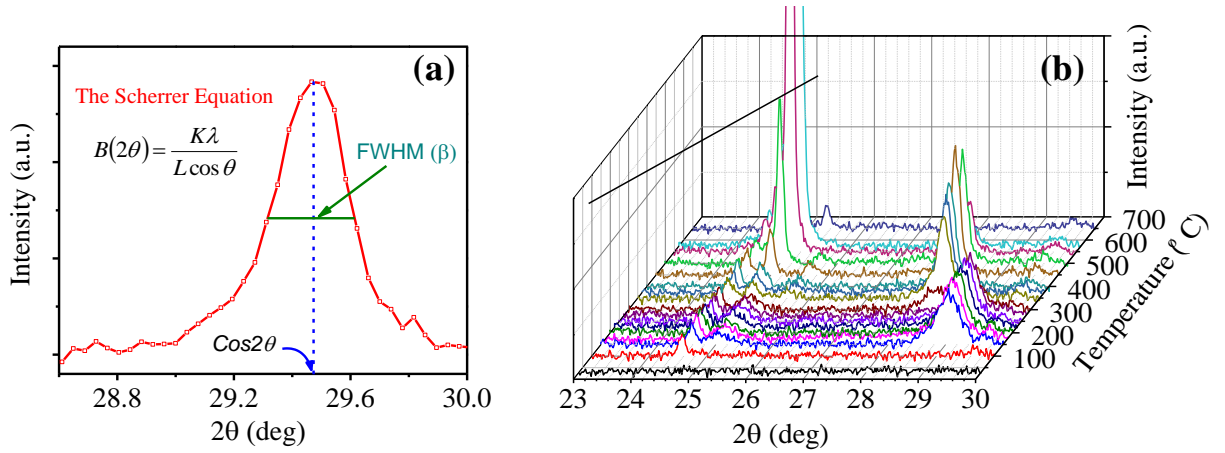


Figure 5.1. X-ray intensity peak from GST thin film at 300 °C. The Scherrer equation is used to calculate average grain size where K is the dimensionless shape factor (~0.9-1),  $\lambda$  is the X-ray wavelength. Peak width ( $\beta$ ) which is Full Width Half Maximum (FWHM) value inversely proportional to crystallite size (L) (a). In-situ XRD patterns of 200 nm thick GST thin film at various chuck temperature (b).

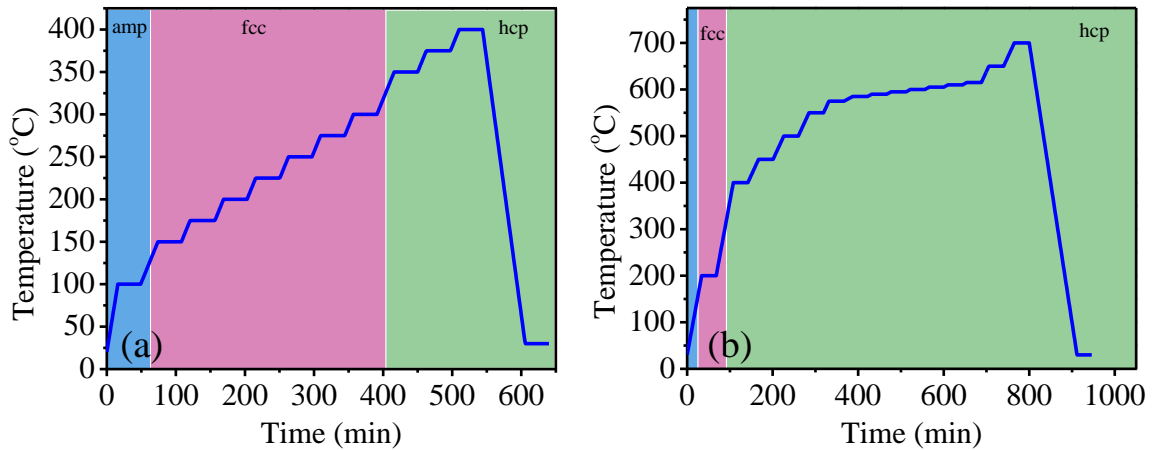


Figure 5.2. In-situ XRD measurement temperature as a function of time up to 400 °C, in 2 °C/min (a) and 700 °C, in decreasing heating rate (5, 2 and 0.5 °C/min) (b). Flat temperature regions are ~ 34 minutes and correspond to the XRD scanning time.

Figure 5.3 shows average grain sizes calculated from in-situ XRD patterns for 200 nm thin film GST at various chuck temperature, and corresponding resistance versus temperature characteristics for a different 200 nm thick GST thin film sample (measured on a different hot chuck setup). Figure 5.2b) shows the same average grain sizes of 200 nm thin film GST together with nucleation rate and growth velocity of GST as a function of temperature [73]. After the material starts crystallizing into *fcc* nucleation and crystal growth are observed in the XRD results as two distinct increases in average grain size: first one occurs at the maximum nucleation rate temperature ( $\sim 325$  °C) and the second one at the maximum growth velocity temperature ( $\sim 460$  °C). Beyond this temperature there is a continuous but slow increase in grain sizes due to slow growth velocity (Figure 5.3 b).

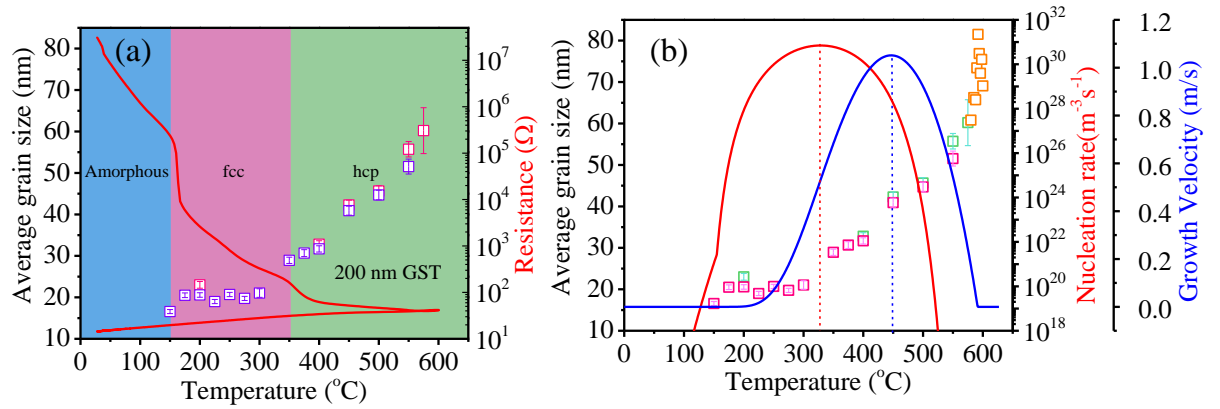


Figure 5.3. Average grain sizes (calculated from in-situ XRD data) and resistances of a different 200 nm thick GST film sample with corresponding phases as a function of chuck temperature (a). Average grain sizes of 200 nm thin film GST with nucleation rate and growth velocity [73] of GST as a function of temperature. Grain sizes are jumping where nucleation rate (also phase change from fcc to hcp) and growth velocity are maximized.

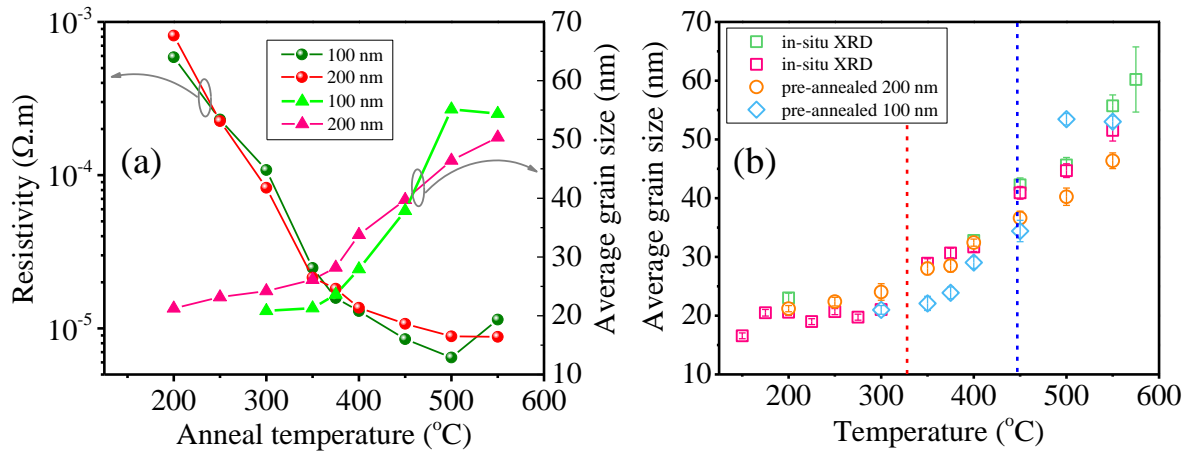


Figure 5.4. Room temperature resistivity and average grain size as a function of anneal temperature for 100 and 200 nm thickness GST films (a). Average grain sizes of two 200 nm films calculated from in-situ XRD measurements (squares) and of 100 nm and 200 nm calculated from (ex-situ) XRD measurements (circle and diamonds) after pre-annealing at the given temperatures (x-axis) for 15 min (b).

### 5.3 Finite Element Simulations

Crystallization dynamics of GST cells are analyzed using COMSOL Multiphysics [71] finite element simulations with planar geometry (Figure 5.5 a) using the electrothermal and crystal density (CD) models referred to previously [70] which include GST nucleation rate and growth velocity parameters from the literature.



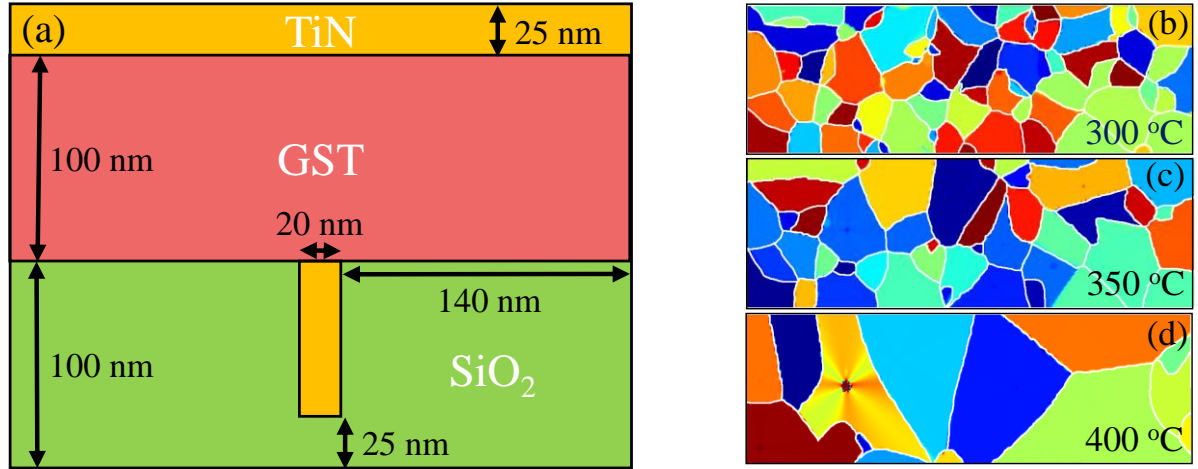


Figure 5.5. Cross section of the planar mushroom cell geometry and materials simulated using COMSOL multiphysics with the electrothermal and CD models mentioned earlier [70] (a). GST region of (20 nm depth) planar mushroom cell with varying crystalline size after 200 ns annealing at 300 °C (b), 350 °C (c), and 400 °C (d). In these simulations the device is annealed at different constant temperatures from  $t=0$  to  $t=200$  ns.

The temperature dependent nucleation and growth functions used in the model lead to different crystalline grain distributions at the different temperatures with larger grain sizes at higher temperatures as expected (Figure 5.5 b,c,d), with ~20, 25, and 45 nm average grain sizes after 200 ns anneal at 300 °C, 350 °C, and 400 °C, respectively. The white lines show the grain boundaries that are modeled between the growing grains. The average grain sizes are obtained from the simulated final grain distributions using the image processing and particle analysis software ImageJ [74].

In Figure 5.6 the average grain sizes obtained from in-situ XRD measurements are plotted together with those from the simulated annealed mushroom cell at different anneal temperatures. The simulated and experimental anneals are quite different and on time-scales that are orders of magnitude apart (simulated 200 ns at a constant temperature

versus hours long temperature ramps for the in-situ XRD measurements) hence comparison of experimental and simulated average grain sizes is not meaningful at this point. Further work is required to simulate experiment-like anneals and use the experimentally obtained grain sizes to calibrate the nucleation and growth rates for the particular material. Due to very low nucleation rate and growth velocity below 200 °C and low nucleation rate above 450 °C no crystallization was observed in the simulations for these temperature regions.

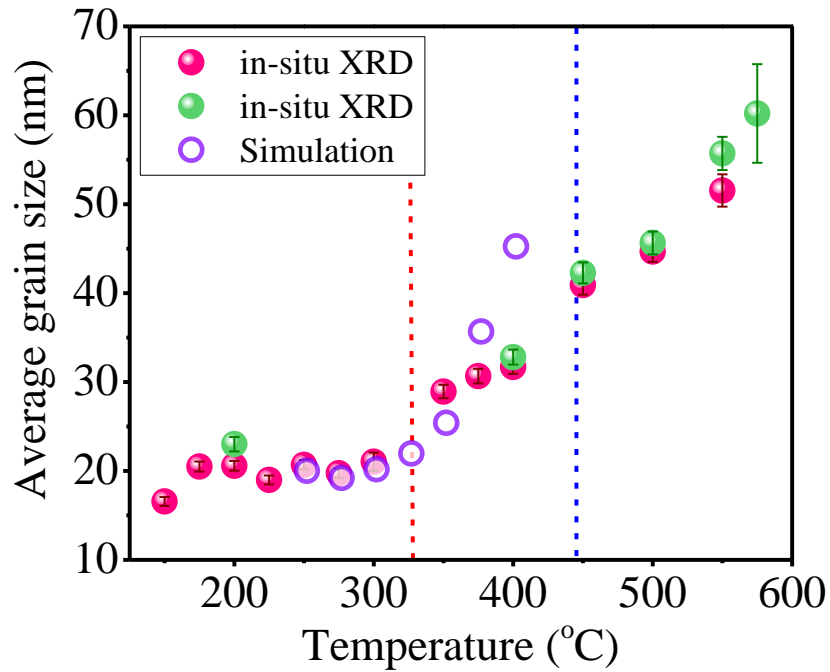


Figure 5.6. Average grain size as a function of anneal temperature obtained from in-situ XRD data for a 200 nm thick GST thin film, ~ 34 minutes at each temperature (solid circles) and from preliminary simulations on GST cells annealed at various, constant anneal temperatures for 200 ns (open circles).

## 6. Conclusion

This work focused on temperature dependent characterization of GeSbTe thin films and nanoscale structures with the goal of contributing to a better understanding of phase-change memory materials and devices.

Electrical resistivity of liquid GST ( $\rho_{\text{GST-Lq}}$ ) was extracted as  $1.26 \pm 0.15 \text{ m}\Omega\cdot\text{cm}$  from thin film measurements and as  $0.31 \pm 0.04 \text{ m}\Omega\cdot\text{cm}$  and  $0.21 \pm 0.03 \text{ m}\Omega\cdot\text{cm}$  from 20 nm and 50 nm thick structures from a large number of measurements on individual GST nanostructures self-heated to melt by single microsecond voltage pulses. Breaking of the thin film in liquid state suggests that thin film measurements overestimate the liquid resistivity value. These first results on nanoscale device level measurements of liquid GST electrical resistivity are in good agreement to those reported for liquid GST measured by melting bulk GST in a macroscopic setup ( $\sim 0.36 \text{ m}\Omega\cdot\text{cm}$  at  $\sim 990 \text{ K}$  with a TCR of  $-0.8 \mu\Omega\cdot\text{cm}/\text{K}$ [33]). The difference could be explained by an average temperature within the liquid GST nanostructures of  $\sim 1056 \text{ K}$  for the 20 nm thick structures and of  $\sim 1170 \text{ K}$  for the 50 nm thick structures, which appear to be reasonable (though not experimentally or computationally confirmable at this point due to lack of experimental techniques or accurate enough models to estimate the temperature distribution within the molten GST nanostructures).

We have compared the crystallization behavior of GST films on silicon nitride and on silicon dioxide through slow resistance versus temperature measurements. While the first phase transition, from amorphous to fcc, is observed at approximately the same temperature for all samples ( $\sim 170 \text{ }^\circ\text{C}$ ), the second phase transition, from fcc to hcp, is observed at  $\sim 260 \text{ }^\circ\text{C}$  for the GST/nitride samples and at  $\sim 340 \text{ }^\circ\text{C}$  for the

GST/oxide samples. Silicon nitride appears to facilitate the fcc-hcp phase-transition of GST and we speculate this may be due to the hexagonal symmetry of silicon nitride [49]. Our results also show the importance of the heating rate in determining phase transition temperatures. Knowledge of the crystallization behavior of GST and how it is affected by different underlying films is important for design of phase-change memory devices.

The effect of the baseline voltage on the crystallization behavior of nanoscale  $\text{Ge}_2\text{Sb}_2\text{Te}_5$  line cells was investigated with experiments and simulations by applying a voltage pulse (melting pulse) with varying baseline voltages. A baseline (offset) voltage can play an important role in the set operation (maintaining a molten filament by melting the amorphous region and utilizing growth-from-melt templated from the crystalline regions). After the melting pulse, the GST wires stay either partially molten (by retaining of a current carrying filament) and recrystallize, or they resolidify as amorphous, depending on the applied baseline. Our electro-thermal models also show the same current-time characteristics and capture the filament formation and crystallization dynamics shown in our experiments.

Finally, XRD measurements on as-deposited amorphous GST thin films were performed in-situ up to high temperatures and ex-situ, at room temperature on pre-annealed samples at various temperatures, to characterize grain size distributions. Average grain sizes of GST were calculated from the XRD data using the Scherrer equation. These results will be used to improve and calibrate our electrothermal and crystallization models which currently use GST nucleation rate and velocity growth parameters available in the literature. Preliminary simulations were performed to show

example grain distributions obtained in mushroom cells annealed at constant temperatures. However, given very different heating conditions in the experiments and simulations, further modeling work is required for a meaningful comparison to the experimental data, which in turn will enable validation and improvement of the models. The relative grain orientations and electrical and thermal grain boundaries resistances may play important roles in the crystallization mechanisms.

The experimental results presented in this thesis are expected to contribute to a better understanding and more accurate models for phase-change memory materials and devices.

## 7. Appendices

### 7.1 Software tools developed using LabVIEW for instrument control for electrical characterization

#### 7.1.1 Pulse generator control program

Agilent 8114A high voltage pulse generator is used in electrical characterization for the GST devices. Pulse generator control program is developed using LabVIEW. Front panel of control program is shown in Figure 7.1. Pulse period, number of pulse, pulse amplitude, pulse width, and offset voltage are defined manually by the user. There are two activation switch for parameter setting and pulse sending to prevent unintentional pulsing to the device. Oscilloscope parameters such as trigger source channel, horizontal and vertical scale for each channel can also be set using the same interface.

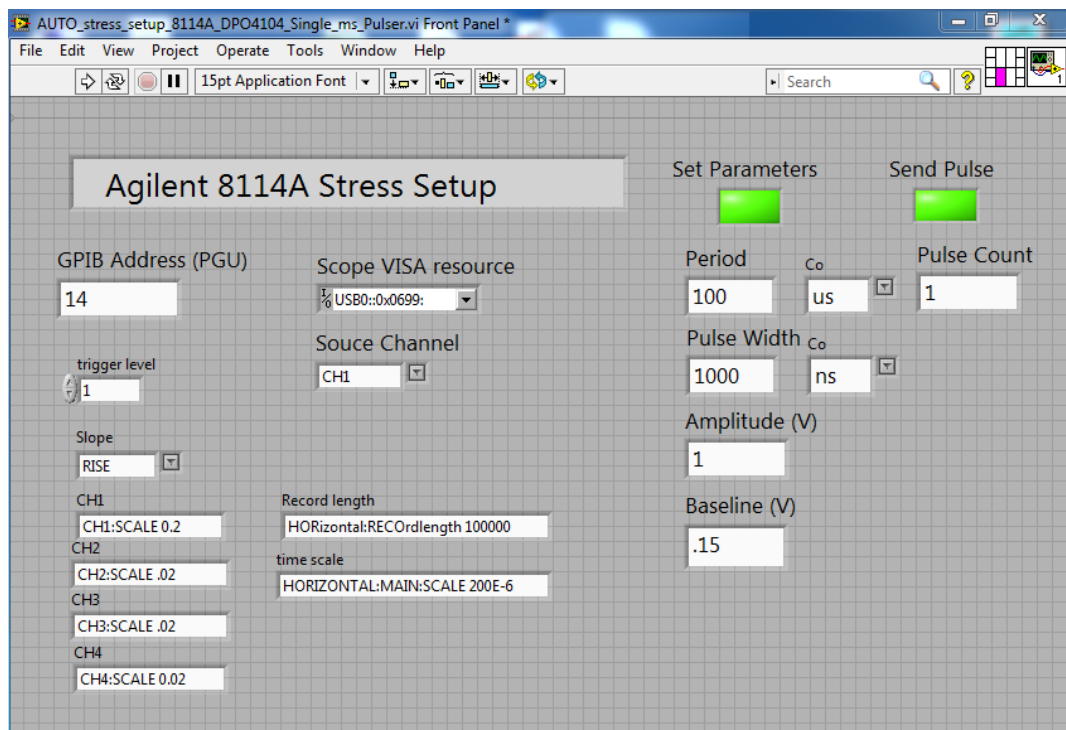


Figure 7.1. Front panel of pulse generator controller tool.

## 7.1.2 Oscilloscope data acquisition program

A computer controlled Tektronix DPO4104 oscilloscope is used to capture applied voltage amplitude and current for electrical characterization. Front panel of control program is shown in Figure 7.2. Measurements are saved with prefix in file path, which is the directory name, adding file number and a suffix of '.txt' to the prefix. The file number is incremented if the counter button is activated by the user. Counter can be reset with reset button to initialize for the new data file name. Preferred channels can be defined (voltage, current, or resistance) and selected by turning on and off “active” buttons for each channel. Resistance is calculated by using voltage and current data. Waveform chart is included to plot the data during acquisition.

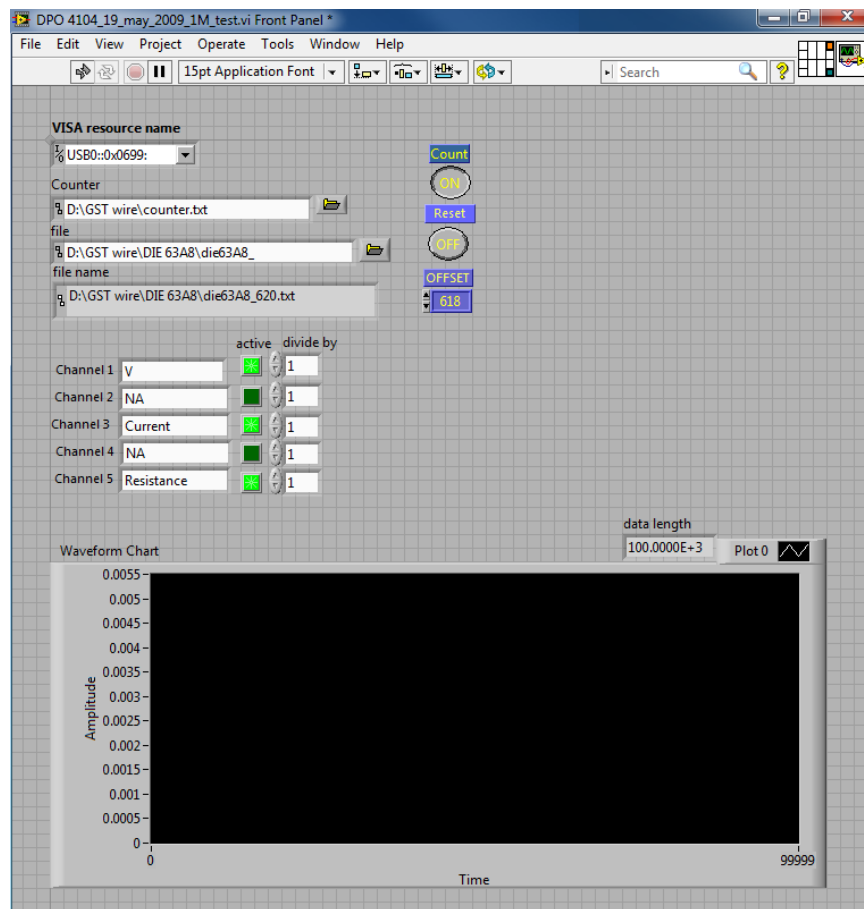


Figure 7.2. Front panel of Tektronix DPO 4104 Oscilloscope data acquisition tool.

### **7.1.3 Cryogenic probe station and temperature controller data acquisition program**

Janis UHT-500 cryogenic probe station and temperature controller are used in electro-thermal characterization of GST devices. Front panel of Janis UHT-500 cryogenic probe station and temperature controller data acquisition program is shown in Figure 7.3. Most of the information such as file names, measurement parameters, and user comments are saved in an index file. Data file name is defined by the user. Control program has 4 inputs and each input can be chosen as silicon diode, positive temperature coefficient resistance temperature detector (PTC-RTD), negative temperature coefficient resistance temperature detector (NTC-RTD), and thermocouple. There are 2 control outputs which controlled by 3 outputs mode (Closed Loop Proportional Integral Derivative (PID) mode, Zone mode, and Open Loop mode). Close loop PID mode is chosen in GST device measurements to control the output which is linked one of the input sensor to give feedback for stabilization to the target temperature. Control outputs are connected to the resistive heaters which will be setup with start, stop and step temperature configurations for the measurement temperatures. Heaters can also be setup with heating rate (high, medium or low) ramp rate (K/min) defined by user. Temperature or the sensor unit of the each channel are shown in indicators and plotted in waveform charts. Maximum threshold temperature for each channel is defined to protect silicon diode sensors which can be withstand up to 450 K. Resistance value is calculated by using semiconductor parameter analyzer that controlled with sub VI in main program.



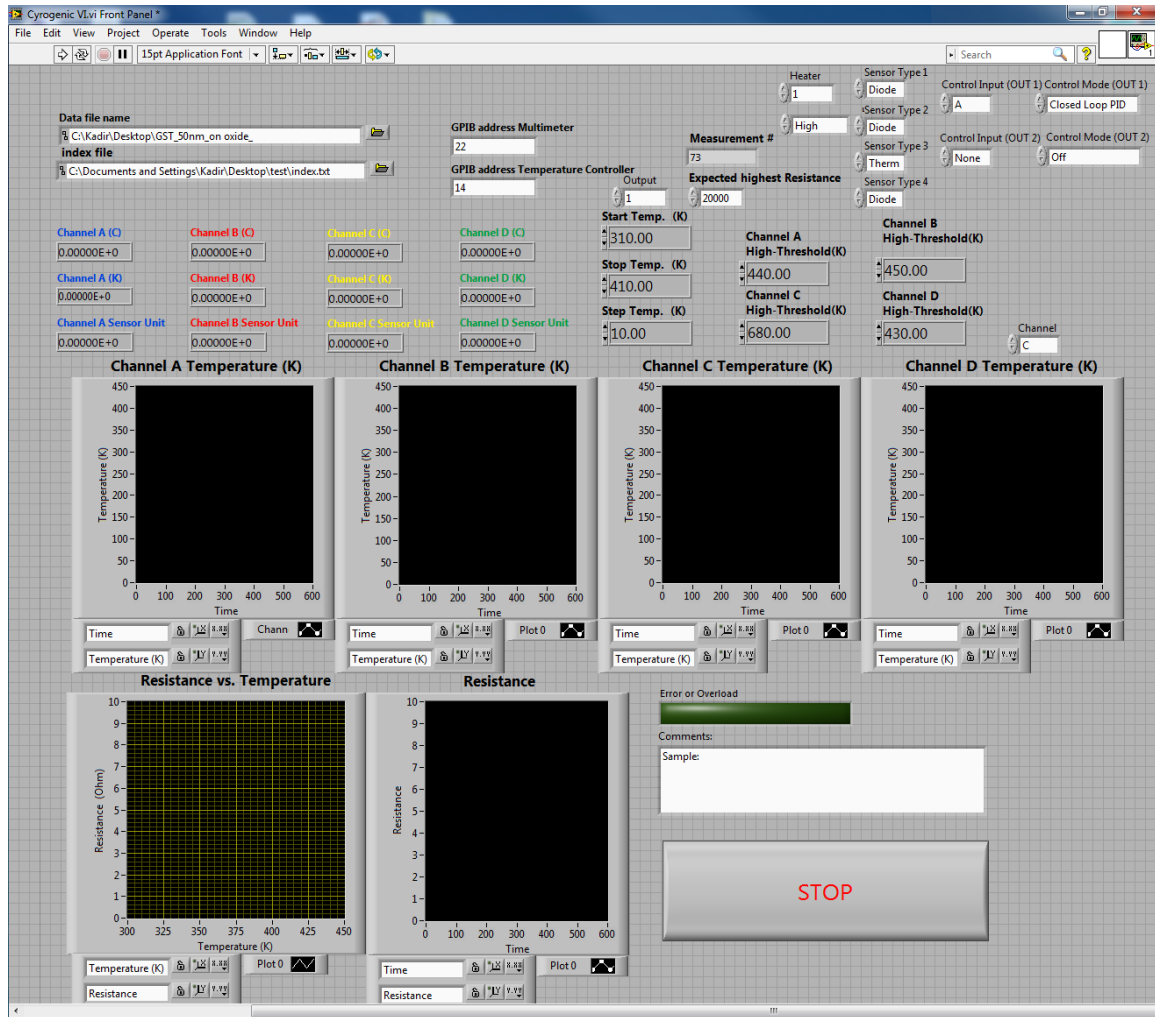


Figure 7.3. Front panel of Janis UHT-500 cryogenic probe station and temperature controller data acquisition tool.

#### 7.1.4 Semiconductor parameter analyzer control program

A computer controlled HP 4145B and Agilent 4156C Parameter analyzers are used for current voltage (I-V) measurement of the GST devices. Front panel of control program is shown in Figure 7.4. The parameter analyzer program is modified version of Ali Gokirmak's parameter analyzer controller program developed for HP 4145B parameter analyzers [75]. Most of the information such as file names, measurement parameters, and user comments are saved in an index file. Measurements are saved with

prefix in file path, which is the directory name, adding file number and a suffix of ‘.data’ to the prefix. The file number is incremented if the counter button is activated by the user. Counter can be reset with reset button to initialize for the new data file name. Parameter analyzer can be set to make single or multiple measurements by turning on and off the “single” button. Multiple measurements can be interrupted by “stop” button. There are 4 source measurement units (SMU) which can be set as voltage, current, ground or constant voltage. The name and plotting function of each SMU can be defined by the user. Control tool have 2 variable voltage settings and one prime voltage setting for the opposite voltage sweep. If the hysteresis button is active, after the measurement, the program changes the parameters for variable 1 to apply a reverse sweep. Measurements can be setup in different time domains by changing the wait and interval time settings.

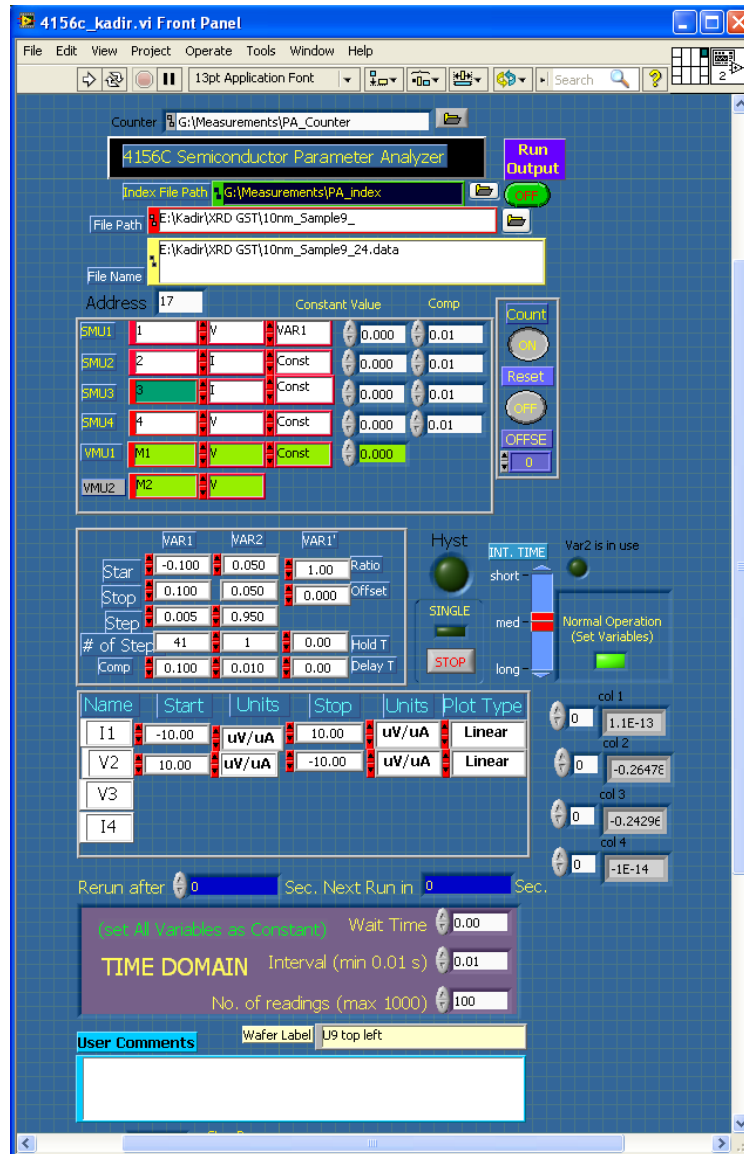


Figure 7.4. Front panel of Agilent 4156C semiconductor parameter analyzer control tool.

## 7.1.5 Semiconductor parameter analyzer data plot and analysis program

Parameter analysis data plot and analysis program is modified version of Ali Gokirmak's MOSFET parameter extraction program. Front panel of control program is shown in Figure 7.5. Program can be either called by the parameter analyzer control

program or run independently to extract the parameters such as slope, resistance, intercept and conductance. Most of the information about extraction of the data such as file names, input values and calculated parameters are saved in a parameter file. Multiple data sets can be plot on top of each other in the same graph by turning off “clear” button or using “counter” button with specified starting and ending data number. 4 point resistance and conductance calculation functions are added for the R-T measurements.

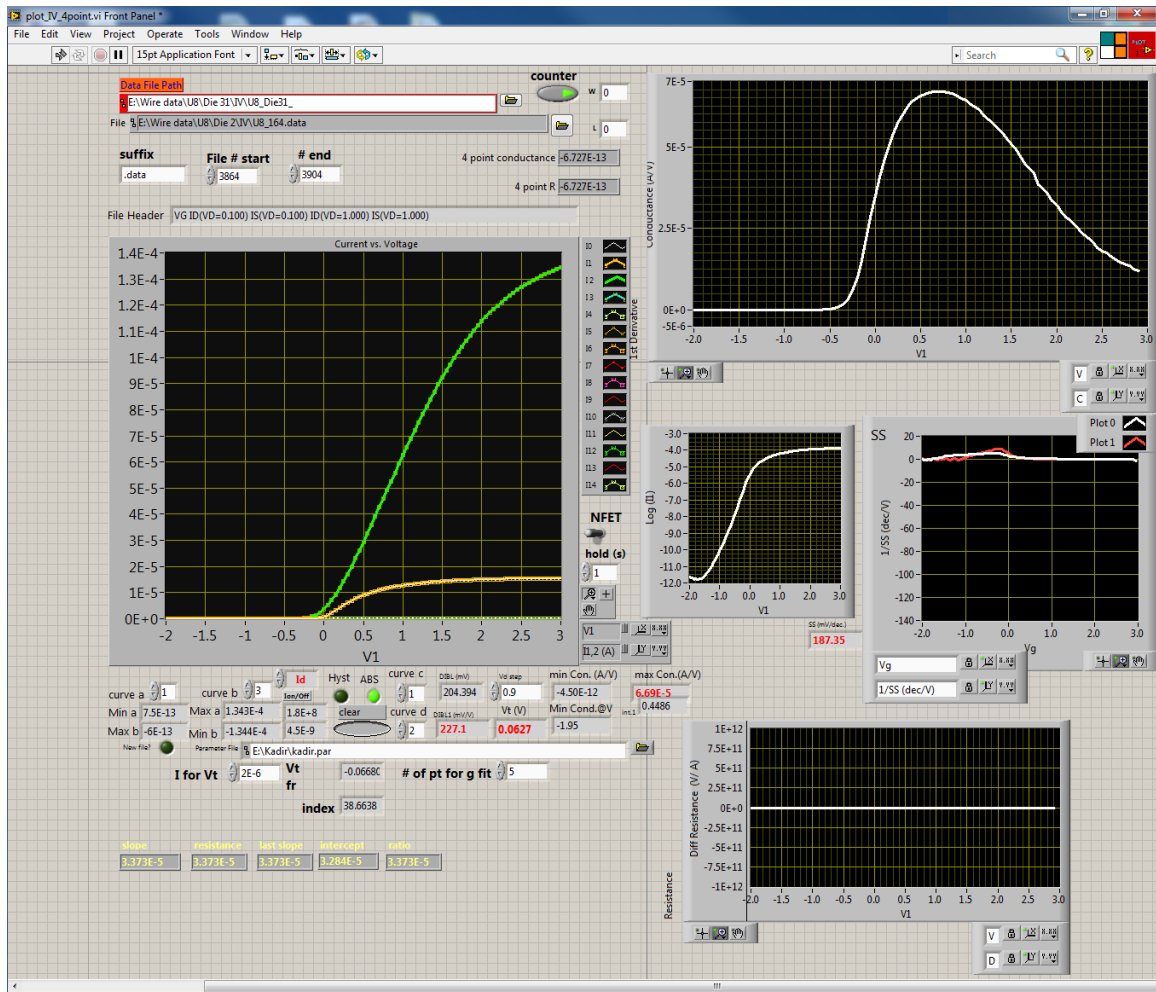


Figure 7.5. Front panel of semiconductor parameter analyzer data plot and analyzer tool.

### **7.1.6 Function generator unit control program**

Tektronix AFG 3102 Dual Channel Arbitrary/Function Generator is used to create arbitrary voltage pulses for electrical characterization of GST devices. Front panel of the control program is shown in Figure 7.6. Most of the information such as file names, measurement parameters and user comments are saved in an index file. Arbitrary signal created with 4 different sections. Pre-pulse section is created to measure initial device resistance. Main pulse section will be setup with start, stop and step configurations for the melting pulse. Post pulse flat section allows device for quenching with defined time and offset value. Post pulse section will setup to observe crystallization of the device at higher temperatures. Oscilloscope parameters such as input impedances, trigger setup, vertical, and horizontal scales can also be set using the same interface. Before applying the signal, waveform has to be loaded to the function generator by activating “reset parameters” button. Due to the max length of the waveform (128 K) which function generator can support, the maximum time scale is defined as 2 ms for the measurements. Hysteresis button provides AC segments after the pulse with the amplitudes are stepped up and then down.

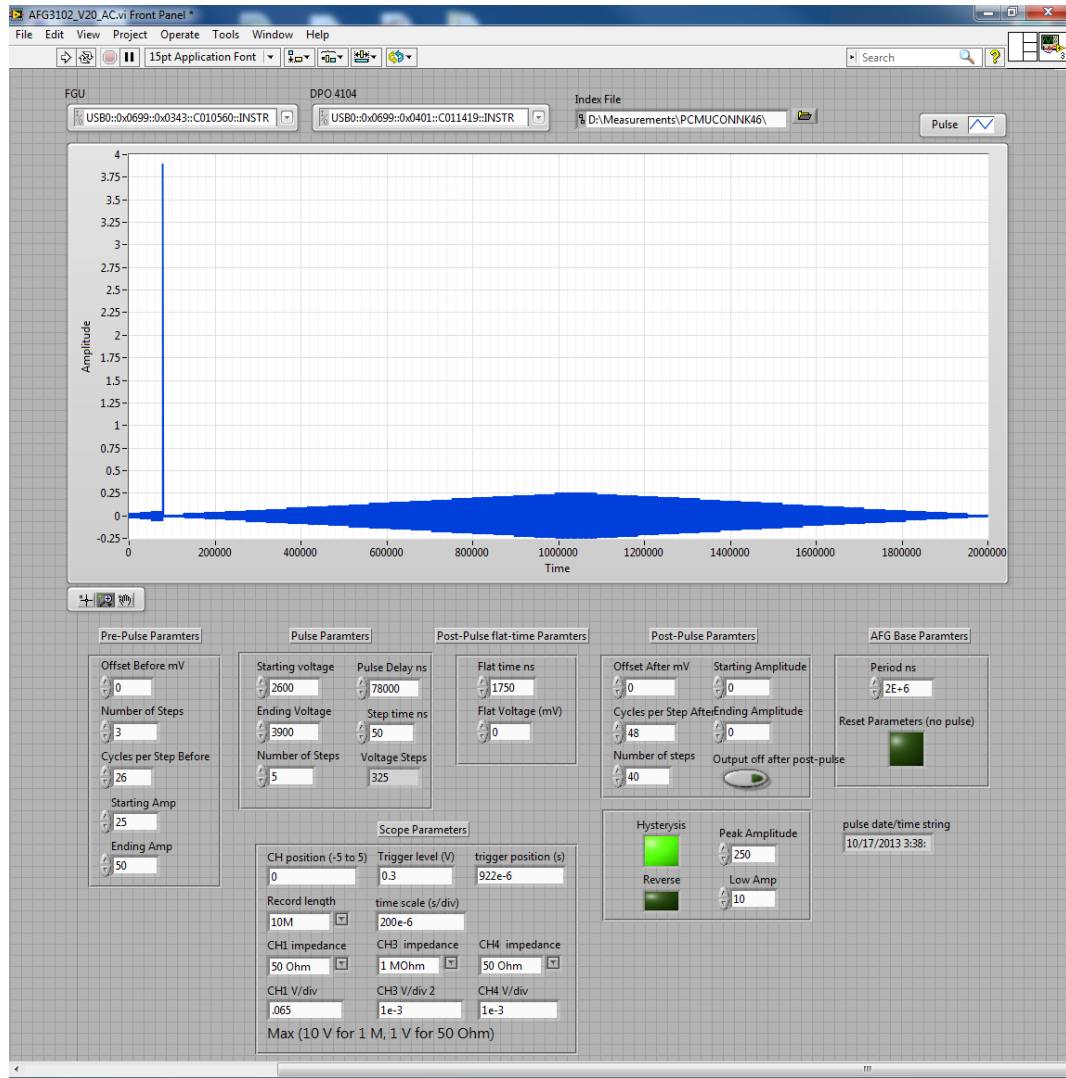


Figure 7.6. Front panel of Tektronix AFG-3102 function generator control tool.

### 7.1.7 Oscilloscope data acquisition program

A computer controlled Tektronix DPO4104 oscilloscope is used to capture applied voltage amplitude and current for electrical characterization. Front panel of control program is shown in Figure 7.7. Waveform chart is included to plot the data during acquisition. This is the updated version of the previous data acquisition program comes with index file, separate wave form chart for each channel, and average offset calculation. Average offsets can be extracted before the measurement by acquiring

constant DC voltage amplitude and calculate average value then subtracted to calibrate the data. If the data length 10 million data points, data is acquired as 10 equal segments sequent by using Matlab code integration into LabVIEW due to the large file size.

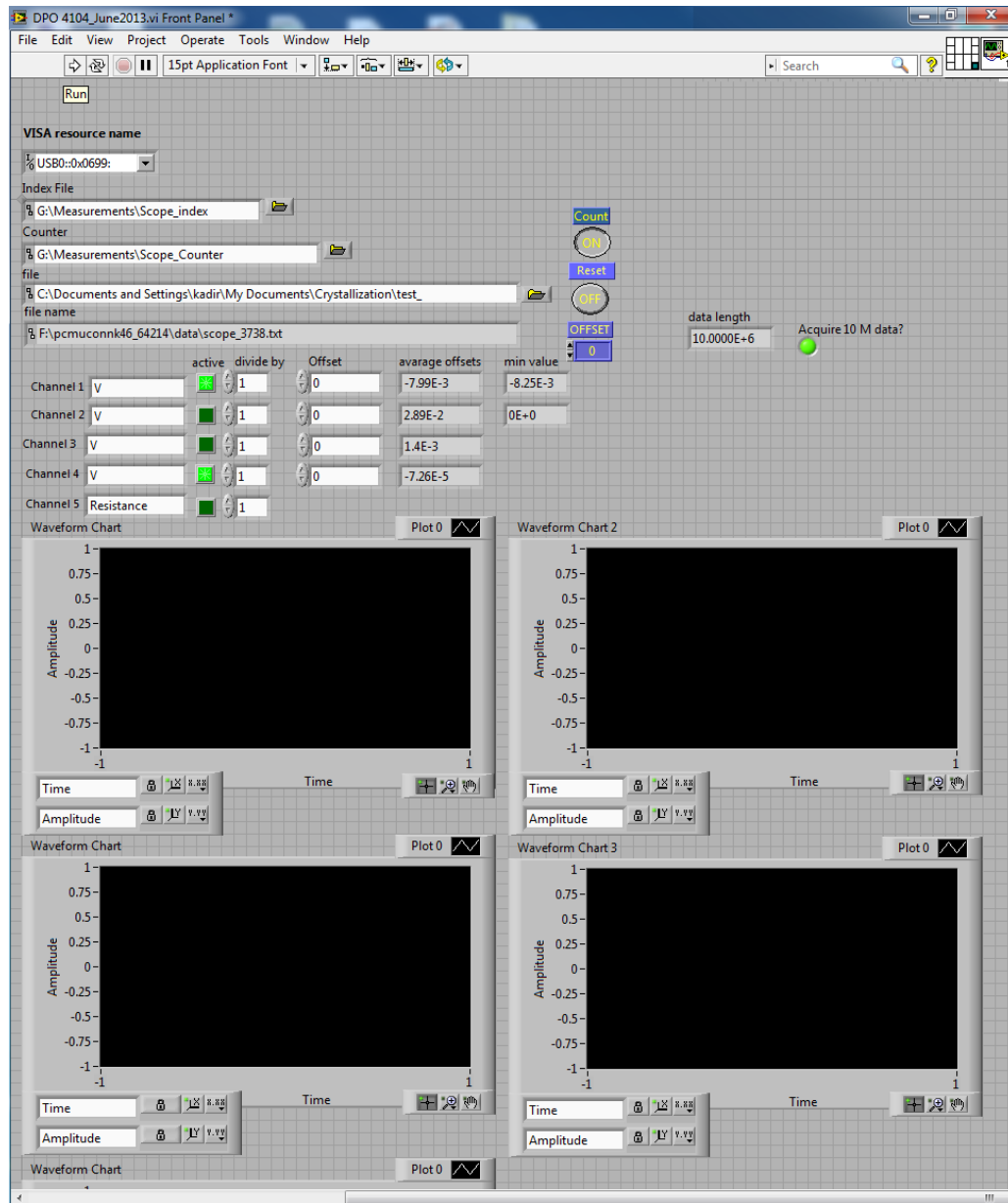


Figure 7.7. Front panel of Tektronix DPO-4104 oscilloscope data acquisition tool.

## 7.2 Optical band gap measurement for amorphous GST thin film

Optical band gap of 100 nm thin film GST was measured by using Ultraviolet (UV) - Near Infrared (NIR) Spectrometer. The optical reflection spectrum of GST film was recorded in the 200-1600 nm wavelength range and the obtained data is shown in Figure 7.8. The optical reflection spectrum of the 100 nm GST thin film is obtained by Agilent Cary 5000 UV-VIS-NIR spectrometer with external Agilent DRA-2500 diffuse reflectance accessory. Reflectance measurements are made by sample on the sphere wall, ensuring efficient collection of a high proportion of diffusely reflected radiation [76].

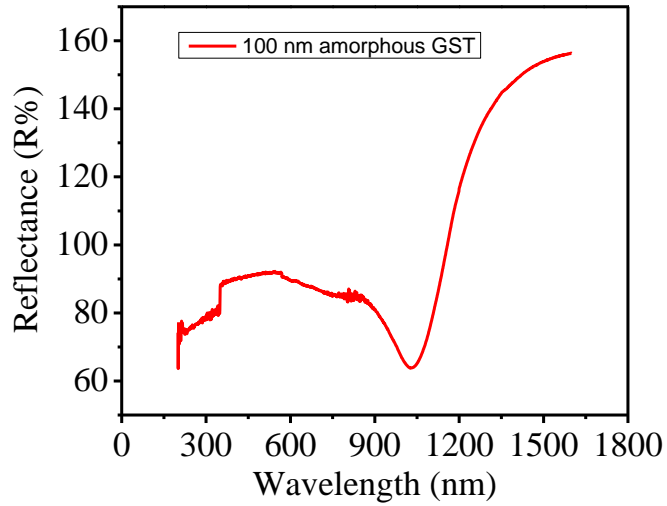


Figure 7.8. Optical reflection spectrum of the 100 nm amorphous GST thin film in 200-1600 nm wavelength range.

The most common models to determine the optical band gap of semiconductors is Tauc model (7.1) which allows us to derive the band gap energy from absorption coefficient and photon energy as a function of incident energy [77]. Energy band gap ( $E_g$ ) in terms of absorption coefficient  $\alpha$  is given by;

$$\alpha h\nu = A\sqrt{(h\nu - E_g)} \quad (7.1)$$



where  $A$  is constant  $h\nu$  is photon energy and  $\alpha$  is absorption coefficient which can be written in terms of reflectance as (7.2);

$$2\alpha t = \ln [(R_{\max} - R_{\min}) / (R - R_{\min})] \quad (7.2)$$

where  $t$  is the thickness of the film and  $R$  is reflectance. Sudden fall in reflectance from  $R_{\max}$  to  $R_{\min}$  is observed due to the absorption of light by the material. The usual method to calculate energy band gap is to plot graph between  $(\alpha h\nu)^{1/2}$  and  $h\nu$  where the intercept of the abscissa indicates the optical band gap.

Figure 7.9 shows reflectance as a function of photon energy for 100 nm GST thin film. In Figure 7.10 the intercept of the abscissa indicates 1.16 eV as optical band gap of the 100 nm amorphous GST thin film.

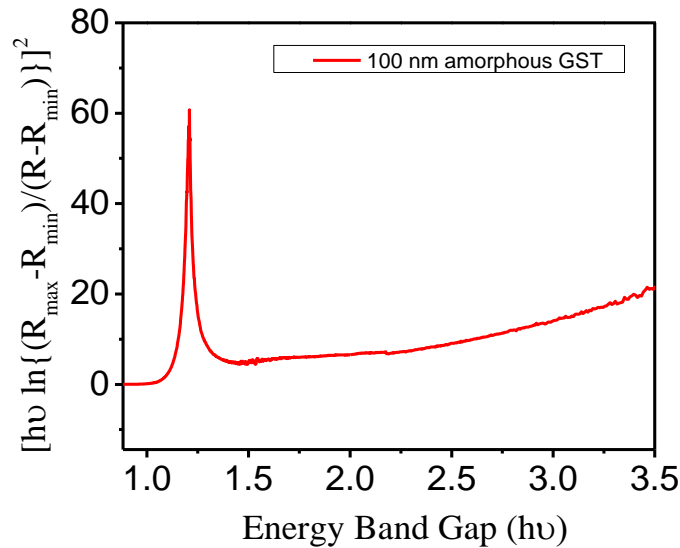


Figure 7.9. Plotting based on the relationship of  $[h\nu \ln \{(R_{\max} - R_{\min}) / (R - R_{\min})\}]^2$  and  $h\nu$  for 100 nm amorphous GST thin film. The intercept in the abscissa indicates an optical band gap of 1.16 eV (inset).

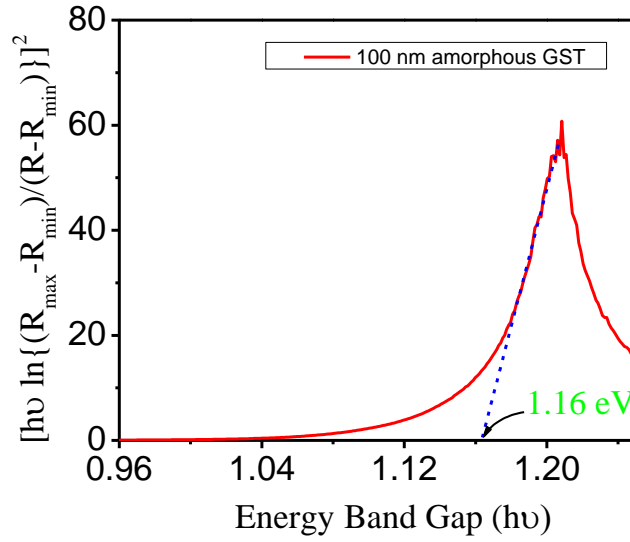


Figure 7.10. Fitting based on the relationship of  $[h\nu \ln \{(R_{\max}-R_{\min})/(R-R_{\min})\}]^2$  and  $h\nu$  for 100 nm amorphous GST thin film. 1.16 eV is determined as optical band gap of the amorphous GST film.

### 7.3 Scanning Auger Microscope Setup

The AES system uses a cylindrical mirror analyzer (CMA). Electron beam ( $2.0 \text{ keV} \leq \text{Kinetic Energy} \leq 10.0 \text{ keV}$ ) originates at  $\text{CeB}_6$  (or  $\text{LaB}_6$ ) ceramic filament. The beam is focused onto a specimen and emitted electrons are deflected around the electron gun and pass through an aperture towards the back of the CMA. Electron beam travels along central axis of energy analyzer, passing through the electron condenser (controlling sample beam current) and objectives lenses (for focusing beam) and finally the octapole deflector (for beam rastering, imaging). After hitting the sample, backscattered and Auger electrons that have the right trajectory pass through the entrance grid and hit the Secondary Electron Detector (SED), where the produced signal is used for imaging the surface. After electrons pass through the entrance grid, they enter the

space between the coaxial cylinders. A negative potential is applied to the outer cylinder, and a smaller negative potential may be applied to the inner cylinder. If the electron kinetic energy varies only slightly from the right value, the electron will pass through the exit grid, pass through an aperture and hit the electron multiplier detector. If the electron energy deviates too much from the right value, it will get lost in the energy analyzer and be absorbed into a metal part (e.g., the inner cylinder). By varying the potentials on the two cylinders (the potentials on the outer and inner cylinders are ramped), the energies of the electrons that can be detected are changed and it allows derivative mode plotting of the Auger data. An optional ion gun can be integrated for depth profiling experiments (Figure 7.11).

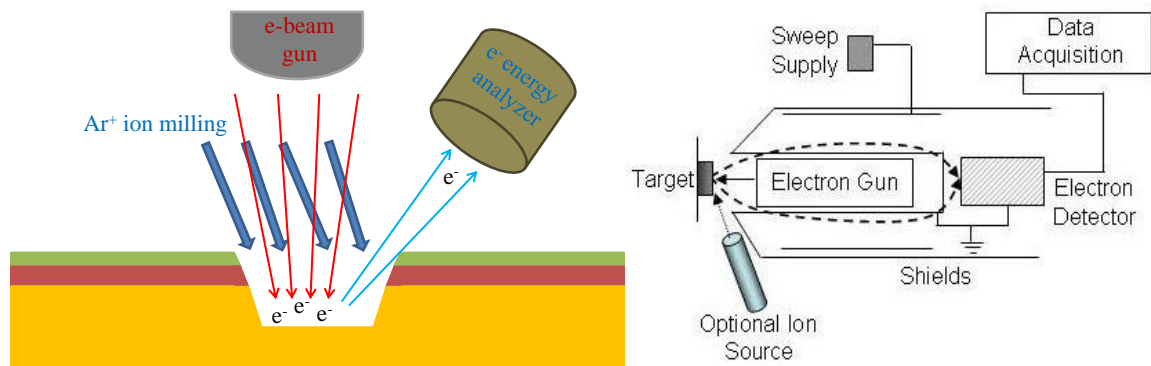


Figure 7.11. Auger depth profiling schematics.

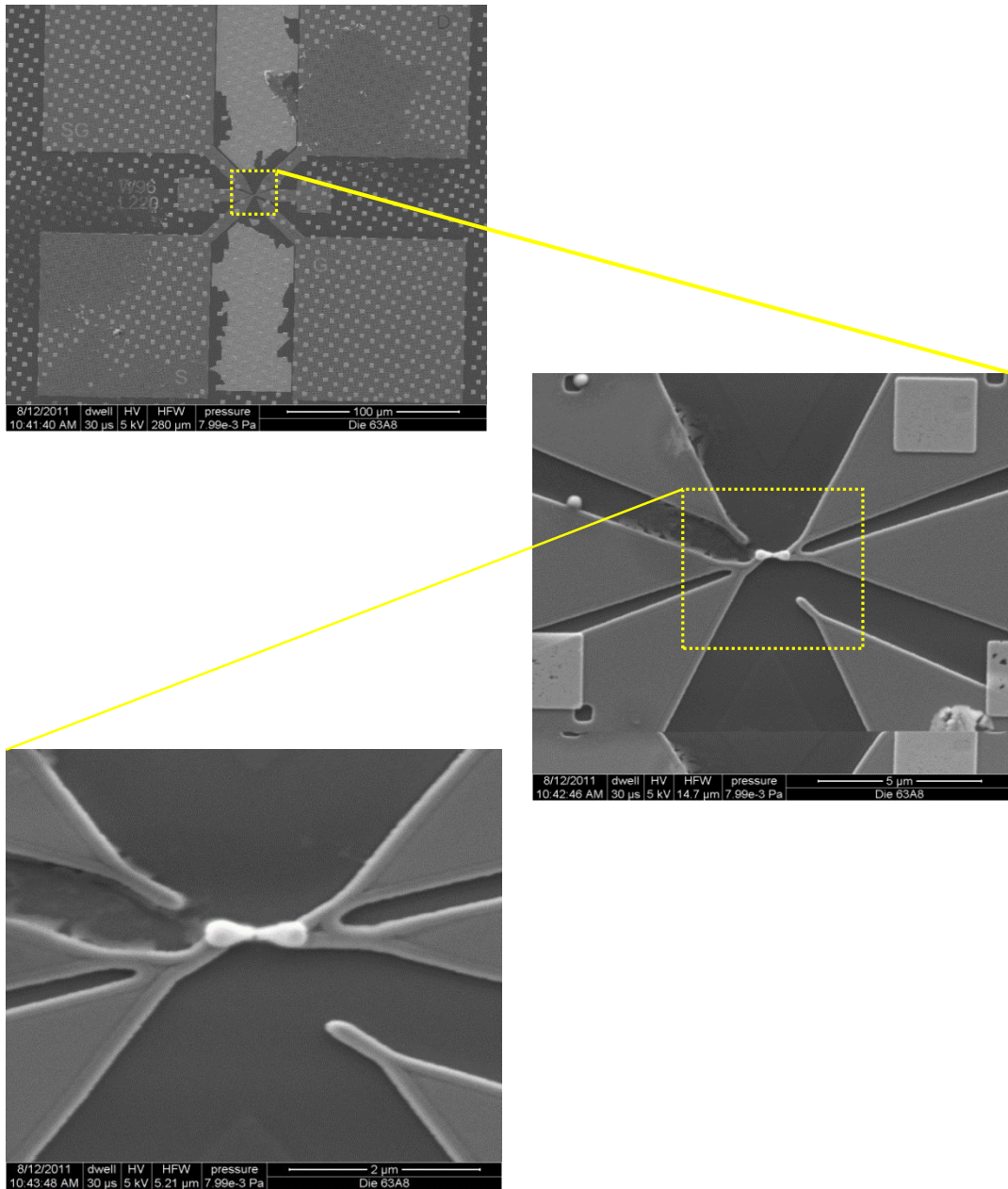


Figure 7.12. SEM images of the pulsed GST device (Width: 96 nm and Length: 220 nm). 100 x 100 µm contact pads are shown in top figure. Higher magnification SEM images shows the metal contact (middle figure) and GST device (bottom figure).

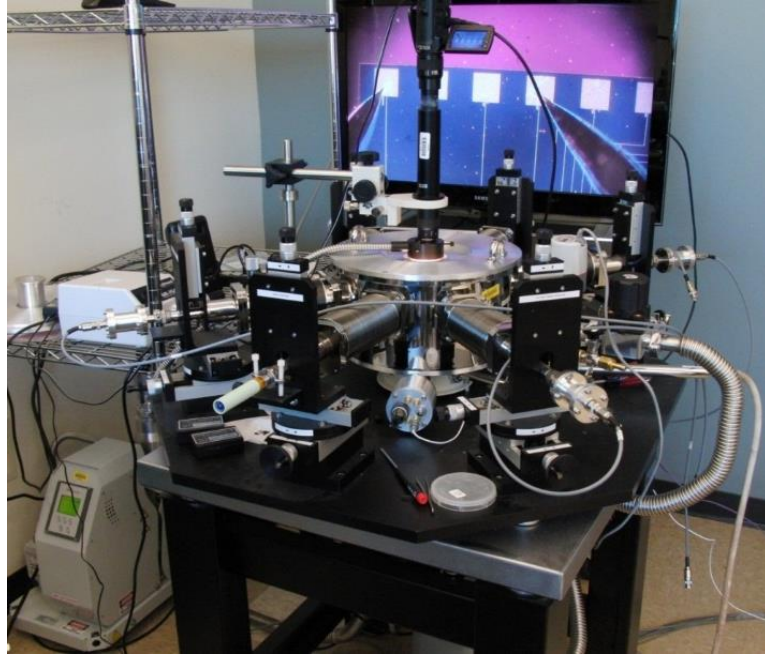


Figure 7.13. Janis UHT-500 cryogenic probe station with turbo pump. Full HD camcorder attached with optical lens and TV are used for positioned the micromanipulator probes.

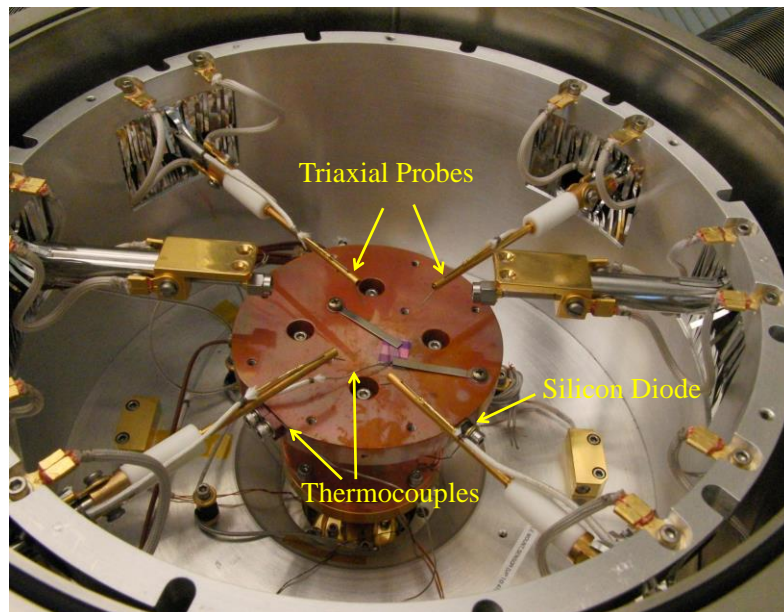


Figure 7.14. Inside of the vacuum chamber and the radiation shield of the cryogenic probe station. Micromanipulators with triaxial probe connections, thermocouples and silicon diode sensor attached to the chuck are shown.

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