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A More Sophisticated Treatment of Collisions

Carl W. David *University of Connecticut*, Carl.David@uconn.edu

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A More Sophisticated Treatment of Collisions

C. W. David Department of Chemistry University of Connecticut Storrs, Connecticut 06269-3060 (Dated: November 5, 2008)

I. FRACTION OF MOLECULES CAPABLE OF COLLIDING

and the number of collisions between A-type and B-type molecules in these velocity ranges per unit time is:

For A-type molecules, we have the fraction of molecules whose velocity components are between v_x and $v_x + dv_x$, etc., as

$$
\frac{dN_A}{N_A} = \left(\frac{m_A}{2\pi kT}\right)^{\frac{3}{2}} e^{-m_A(v_x^2 + v_y^2 + v_z^2)/(2kT)} dv_x dv_y dv_z
$$
\n(1.1)

and for B-type molecules, we have

$$
\frac{dN_B}{N_B} = \left(\frac{m_B}{2\pi kT}\right)^{\frac{3}{2}} e^{-m_B (v_u^2 + v_v^2 + v_w^2)/(2kT)} dv_u dv_v dv_w
$$
\n(1.2)

$$
dZ_{AB} = \frac{dN_A dN_B}{V^2} \pi d_{AB}^2 c_{AB} \tag{1.3}
$$

where

$$
c_{AB} = \sqrt{(v_x - v_u)^2 + (v_y - v_v)^2 + (v_z - v_w)^2}
$$

Adding up all the collisions over all velocity ranges gives:

Z N^A N^B m^B ³/² m^B ³/² Z Z Z dZAB = πd² dv^x dv^y dv^z dv^u dv^v dv^w AB V V 2πkT 2πkT q 2 2 2 2 2 2 −mA(v ^x+v ^y+v)/(2kT)−mB(v ^u+v ^v+v ^w)/(2kT) e (v^x − vu) ² + (v^y − vv) ² + (v^z − vw) 2 z

To proceed with the integration, it is convenient to convert to the center of mass coördinate system where

$$
\dot{X}_{c.of.m.} = \frac{m_A v_x + m_B v_u}{m_A + m_B} = \delta
$$

$$
\dot{Y}_{c.of.m.} = \frac{m_A v_y + m_B v_v}{m_A + m_B} = \zeta
$$

$$
\dot{Z}_{c.of.m.} = \frac{m_A v_z + m_B v_w}{m_A + m_B} = \eta
$$

$$
\dot{x}_{AB} = v_x - v_u \equiv \alpha
$$

$$
\dot{y}_{AB} = v_y - v_v \equiv \beta
$$

$$
\dot{z}_{AB} = v_z - v_w \equiv \gamma
$$

we can get the new differential volume element using the Jacobian (see Appendix), i.e.,

$$
dv_x dv_y dv_z dv_u dv_v dv_w =
$$

$$
J(\alpha, \delta)J(\beta, \zeta)J(\gamma, \eta) d\alpha d\beta d\gamma d\delta d\zeta d\eta
$$

Typeset by REVTEX

and

where each Jacobian looks like the first, i.e.,

$$
J(\alpha, \delta) = \begin{vmatrix} \frac{\partial \alpha}{\partial v_x} & \frac{\partial \delta}{\partial v_x} \\ \frac{\partial \alpha}{\partial v_u} & \frac{\partial \delta}{\partial v_u} \end{vmatrix}
$$

$$
= \begin{vmatrix} 1 & \frac{m_A}{\alpha + m_B} \\ -1 & \frac{m_B}{m_A + m_B} \end{vmatrix} = 1
$$

so

$$
\int dZ_{AB} = \pi d_{AB}^2 \frac{N_A}{V} \frac{N_B}{V} \left(\frac{m_B}{2\pi kT}\right)^{3/2} \left(\frac{m_B}{2\pi kT}\right)^{3/2}
$$

$$
\int d\alpha \int d\beta \int d\gamma \int d\delta \int d\zeta \int d\eta
$$

$$
e^{-\mu(\alpha^2 + \beta^2 + \gamma^2)/(2kT) - (m_A + m_B)(\delta^2 + \zeta^2 + \eta^2)/(2kT)}
$$

$$
\sqrt{\alpha^2 + \beta^2 + \gamma^2}
$$

$$
\int dZ_{AB} = \pi d_{AB}^2 \frac{N_A}{V} \frac{N_B}{V} \left(\frac{m_B}{2\pi kT}\right)^{3/2} \left(\frac{m_B}{2\pi kT}\right)^{3/2}
$$

$$
\int d\alpha \int d\beta \int d\gamma \sqrt{\alpha^2 + \beta^2 + \gamma^2} e^{-\mu(\alpha^2 + \beta^2 + \gamma^2)/(2kT)}
$$

$$
\int d\delta \int d\zeta \int d\eta e^{-(m_A + m_B)(\delta^2 + \zeta^2 + \eta^2)/(2kT)}
$$

where all integrals are over the range from $-\infty \to +\infty$. We then have, since they are all standard integrals

$$
\int dZ_{AB} = Z_{AB} = \pi d_{AB}^2 \frac{N_A}{V} \frac{N_B}{V} \left(\frac{m_A}{2\pi kT}\right)^{3/2}
$$

$$
\left(\frac{m_B}{2\pi kT}\right)^{3/2} \left(\left(\frac{2\pi kT}{m_A + m_B}\right)^{1/2}\right)^3 8\pi \left(\frac{kT}{\mu}\right)^2
$$

and employing

$$
\frac{1}{m_A}+\frac{1}{m_B}=\frac{1}{\mu}
$$

one obtains (ρ is the number density!)

$$
Z_{AB} = \pi d_{AB}^2 \rho_A \rho_B \left(\frac{\sqrt{\mu}}{2\pi kT}\right)^3 8\pi \left(\frac{kT}{\mu}\right)^2 \tag{1.4}
$$

which is

$$
Z_{AB} = \pi d_{AB}^2 \rho_A \rho_B \sqrt{\frac{8kT}{\pi \mu}} \tag{1.5}
$$

For a pure A system, $\mu = m_A/2$ and $\rho_A = \rho_B = \rho$, and dividing by two to avoid the double count, one has

$$
Z_{AA} = \frac{\pi d^2 \rho \sqrt{2}}{2} \sqrt{\frac{8kT}{\pi m_A}}
$$
(1.6)

II. MOLECULES COLLIDING WITH A WALL

The volume of the cylinder constructed in the figure is

$cdt \cos \vartheta dS$

and the number of molecules in that volume is

$\rho c dt \cos \vartheta dS$

where ρ is the number density. The fraction of those molecules which have the correct (appropriate) angle, and speed to actually strike the differential element of surface area on the wall, dS , in time dt is

$$
\rho c dt \cos \vartheta d S K e^{-mc^2/(2kT)} c^2 dc \sin \vartheta d\vartheta d\varphi
$$

where K is the normalization constant.

$$
dN = [\rho(c \cos \vartheta)]Ke^{-mc^2/(2kT)}c^2dc \times \sin \vartheta d\vartheta d\varphi (dSdt)
$$

i.e.,

$$
\int \frac{dN}{dSdt} = \rho K \int_0^{2\pi} d\varphi \int_0^{\pi/2} \cos \vartheta \sin \vartheta d\vartheta
$$

$$
e^{-mc^2/(2kT)} c^3 dc
$$

FIG. 1: Cylinder containing molecules which will collide with dS in time dt

Since

$$
\int_0^{\pi/2} \cos \vartheta \sin \vartheta d\vartheta = -\left. \frac{\cos^2 \vartheta}{2} \right|_0^{\pi/2} = \frac{1}{2}
$$

and

$$
\int_0^{2\pi} d\varphi = 2\pi
$$

we have

$$
\frac{dN}{dSdt} = \frac{1}{4\pi} \frac{1}{2} \overline{c}(2\pi) = \frac{\rho \overline{c}}{4}
$$

III. APPENDIX

From elementary calculus, as example, the Jacobian connecting Cartesian to polar coördinates (in the plane) proceed from the definitions:

$$
x = r \cos \varphi
$$

and

$$
y=r\sin\varphi
$$

so

$$
\frac{\partial(x,y)}{\partial(r,\varphi)} = J = \begin{vmatrix} \frac{\partial x}{\partial r} & \frac{\partial x}{\partial \varphi} \\ \frac{\partial y}{\partial r} & \frac{\partial y}{\partial \varphi} \end{vmatrix} = \begin{vmatrix} \cos\varphi & -r\sin\varphi \\ \sin\varphi & r\cos\varphi \end{vmatrix} = r
$$

so $dxdy = rdrd\varphi$.